

(19)



Europäisches Patentamt

European Patent Office

Office européen des brevets



(11)

EP 0 548 975 B1

(12)

EUROPEAN PATENT SPECIFICATION

(45) Date of publication and mention
of the grant of the patent:

11.06.1997 Bulletin 1997/24

(51) Int Cl.⁶: **H01Q 1/24**

(21) Application number: **92121952.3**

(22) Date of filing: **23.12.1992**

(54) **Portable radio and telephones having notches therein**

Tragbare Funk- und Funktelefongeräte mit Schlitzten darin

Appareils de radio et radiotéléphones portables avec des fentes dans ceux-ci

(84) Designated Contracting States:
DE FR GB IT

(30) Priority: **26.12.1991 JP 343794/91**
27.03.1992 JP 100139/92

(43) Date of publication of application:
30.06.1993 Bulletin 1993/26

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- **TRANSACTIONS OF THE INSTITUTE OF ELECTRONICS, INFORMATION AND COMMUNICATION ENGINEERS OF JAPAN vol. E74, no. 6, June 1991, TOKYO JP pages 1547 - 1555 YAMADA ET AL 'Base and Mobile Station Antennas for Land Mobile Radio Systems'**
- **PATENT ABSTRACTS OF JAPAN vol. 011, no. 212 (E-522)9 July 1987 & JP-A62 034 404**
- **PATENT ABSTRACTS OF JAPAN vol. 009, no. 328 (E-369)24 December 1985 & JP-A-60 160 229**
- **PATENT ABSTRACTS OF JAPAN vol. 010, no. 170 (E-412)17 June 1986 & JP-A-61 021 602**
- **PATENT ABSTRACTS OF JAPAN vol. 011, no. 212 (E-522) 9 July 1987 & JP-A-62 034 405**

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EP 0 548 975 B1

Description

The present invention relates to portable radio equipment and is applicable to portable radios or telephones.

Portable radio equipment is described in "Base and Mobile Station Antennas for Land Mobile Radio Systems" by Yamada et al., published in Transactions of the Institute of Electronics, Information and Communication Engineers of Japan, vol. E 74, no. 6, June 1991, Tokyo/JP, pages 1547-1555, and in JP-A-62 034 404, JP-A-62 034 405, and JP-A-60 160 229.

In conventional portable radios, an external electromagnetic wave influence causes an internal system such as a transmitting unit and a receiving unit to malfunction and to deteriorate a transmitting performance. Therefore, in order to avoid such a problem, there is provided an electric shield of a metallic nature in a conducting body of the portable radio equipment so as to cut off the external electromagnetic wave influence.

However, it is confirmed by the inventors of the present invention that a high-frequency current flowing through the electric shield causes an adverse effect on a radiation pattern which is radiated from an antenna of the portable radio. It is presumed that a vertically polarized wave among the electromagnetic wave is relatively large and thus it is likely to be favorable that a gain of the vertically polarized wave in the vertical direction is large.

An example of the conventional portable radio equipment where the electric shield is provided is shown in FIG. 1. In the same figure, the reference numeral 102 shows a housing serving as the electric shield, and the reference numeral 103 shows an antenna. A simulation for the radiation characteristics of the electromagnetic wave in the radio-frequency of an L band is carried out using a model of the portable radio shown in FIG. 1. With reference to FIG. 1, dimensions for the housing 102 are that a width thereof is 0.4λ , a depth 0.15λ and a height 0.5λ , where λ indicates a wavelength. The simulation is carried out using a small-sized model which is equipped with a $\lambda/4$ -monopole antenna and whose antenna can interface with a feeder without a matching circuit. A result of the simulation is shown in FIG. 2.

FIG. 2 shows the calculated result of the radiation pattern of the vertically polarized wave around the antenna being placed in the center with respect to (A) x-z plane, (B) x-y plane and (C) y-z plane. As shown in FIG. 1, an x coordinate is placed in a width direction, a y coordinate is in a depth direction and a z coordinate is in a parallel direction to an axis of the $\lambda/4$ -monopole antenna. The electromagnetic simulator for arbitrary models is made on a super-computer employing a spatial network method. An electromagnetic field in the vicinity of the model was calculated by applying the simulator to an ordinary portable telephone model for the L band. A parameter for three dimensional lattice network is $80 \times 70 \times 90 (\Delta d)$, where a unit length of the lattice, Δd , is

$\lambda/40$. A farfield radiation pattern is calculated from the electromagnetic field on a surface of a closed-area over the model.

Referring to a result of the simulation pattern, the radiation pattern for the x-y plane (B) which shows a pattern for a cross section vertical to the antenna is omnidirectional (radiate the same in all directions). On the other hand, in the radiation pattern with respect to the y-z plane (C), a maximum radiation direction is indicated at approximately 50 degrees tilted from a y axis against a z axis and in a negative z-axis direction. As a result of normalization by a maximum radiation gain (a normalized pattern is a dimensionless number with a maximum value of unity), the radiation pattern with respect to the y-z plane (C) indicates a characteristic of deterioration by approximately 5 dB from the maximum radiation gain, compared to the maximum radiation gain on the x-z plane.

FIG. 3 shows respective radiation patterns which are theoretically optimum, corresponding to FIG. 2.

However, in a $\lambda/2$ -dipole antenna, the maximum radiation direction shall theoretically lie in 90 degrees from an antenna axis in the plane including the antenna axis. Therefore, the fact that the maximum radiation direction is deflected as observed in the radiation pattern of the y-z pattern (C) as the above simulation result demonstrates that the radiation pattern of the antenna itself is affected and disturbed by the radio-frequency current flowing through the electrically shielded housing 102.

Since a large radio-frequency current may flow through the housing due to current distribution of the antenna itself, the radiation pattern is much affected in the $\lambda/4$ -monopole antenna. When the height of housing is converted to a corresponding electrical length and the converted electrical length is approximately equal to the electromagnetic wavelength, a current whose phase is opposite to the radio-frequency current flows on the antenna. As a result, the radiation pattern in the horizontal direction in the portable radio is cancelled out against each other, thus causing to deteriorate the radiation gain in the horizontal direction. In this connection, when the portable radio is designed, without considering an effect of the housing, by calculating the radiation pattern with respect to the antenna alone, a desired electromagnetic radiation pattern can not be obtained because of the influence of the housing even if the portable radio is designed such that the maximum radiation shall be obtained in 90 degrees against the antenna axis.

FIG. 4 shows a model of a portable radio equipment employing an inverted F antenna. In the same figure, the reference numeral 103 designates an antenna, the reference numeral 106 is a short-circuit wire, and the reference numeral 106 designates a feeder for a signal. FIG. 5 shows a calculated result of a radiation gain pattern for the model. In this case, too, a maximum radiation direction in a radiation pattern of a (C) y-z plane is deflected from the horizontal direction (y-axis direction), thus indicating that the radio-frequency current flowing

through the housing affects to deteriorate the radiation pattern.

As described above, though the electric shield is provided to cut off the influence by the external electromagnetic wave, conventionally there exists a problem where the radiation characteristic of antenna alone is disturbed by the radio-frequency current flowing through the housing and thus the desirable radiation characteristic for the portable radio can not be obtained.

It is an object of the present invention to provide a portable radio equipment capable of reducing affect caused by radio-frequency currents flowing through shielding means such as a housing and thus capable of improving a radiation pattern thereof.

According to the invention, there is provided portable radio equipment provided with an antenna for transmitting and receiving electromagnetic waves, a housing on which the antenna is mounted and having a notch therein, said housing being made of an electromagnetic shielding material, and an internal circuit connected to the antenna for generating and receiving the electromagnetic waves through the antenna,

characterized in that

the notch is arranged in the housing in a manner to modify the radiation pattern caused by radio frequency currents flowing on the housing.

Other features and advantages of the present invention will become apparent from the following description taken in conjunction with the accompanying drawings, in which:

FIG. 1 shows an example of the conventional portable radio equipment; FIG. 2 shows calculated results of the radiation pattern of the vertically polarized wave around the antenna being placed in the center with respect to x-z plane (FIG. 2A), x-y plane (FIG. 2B) and y-z plane (FIG. 2C) in the conventional practice;

FIG. 3 shows respective radiation patterns which are theoretically optimum, corresponding to FIG. 2; FIG. 4 shows a model of a conventional portable radio employing an inverted F antenna.

FIG. 5 shows a calculated result of a radiation gain pattern for the model shown in FIG. 4. FIG. 6 shows a portable radio equipment according to the first embodiment for the present invention.

FIG. 7 shows a current distribution on the portable radio, indicated with broken lines, where there is provided the notch in the housing shown in FIG. 6. FIG. 8 shows a model of the portable radio where there is provided the notch in the housing, in order to perform a simulation.

FIG. 9 shows the radiation pattern obtained from the above model shown in FIG. 8.

FIG. 10 shows a portable radio using an inverted F antenna, the portable radio having a notch therein.

FIG. 11 shows a portable radio using a miniature antenna 103 placed over the top surface of the port-

able radio.

FIG. 12 shows a portable radio using a helical antenna.

FIG. 13 shows another example of the portable radio where a range of antenna length ℓ' varies from approximately $3/5 \lambda$ to $3/10 \lambda$ and the notch 101 is provided at a distance ℓ from the feed point to the notch.

FIG. 14 shows still another example of the portable radio where the antenna is provided in a center of a top of the housing.

FIGS 15 through 18 show the radiation patterns in relation to the length a of notch for a being $3/16 \lambda$, $1/5 \lambda$, $1/4 \lambda$, and $1/3 \lambda$, respectively.

FIG. 19 shows a model of the portable radio where the notch is located at a distance ℓ from the feed point of the antenna, the length of antenna is 0.25λ , the width of the housing 102 is 0.4λ , and the depth of the housing 102 is 0.15λ , and the length of notch is 0.25λ .

FIGS 20 through 24 show the radiation patterns in relation to the positions of notch with the distance ℓ being $1/16 \lambda$, $5/48 \lambda$, $3/16 \lambda$, $1/4 \lambda$ and $5/16 \lambda$, respectively.

FIG. 25 shows a portable radio where there are provided two notches in the same side of the housing. FIG. 26 shows an example of the portable radio where there are provided two notches one of which is provided from a side of the housing while the other notch is provided in the opposite side of the housing.

FIG. 27 shows a portable radio equipment having an L-shaped notch. FIG. 28 shows a portable radio equipment having a T-shaped notch. FIG. 29A shows directions of the current flowing around an I-shaped notch. FIG. 29B shows directions of the current flowing around the L-shaped notch. FIG. 29C shows directions of the current flowing around the T-shaped notch.

FIG. 30 shows a portable radio equipment having a longitudinally tilted notch.

FIG. 31 shows a portable radio equipment having a smoothly curved notch.

FIG. 32 shows a portable radio equipment having a notch 101 where there is provided a coil or a ferrite ring in the notch.

FIG. 33 shows a portable radio equipment having a notch 101 where there is provided an optical fiber 204 for communicating a signal between an upper portion of the housing and a lower portion of the housing.

FIG. 34 shows a portable radio equipment utilizing a high resistance wire in place of the optical fiber shown in FIG. 33.

FIG. 35 shows a portable radio equipment where whole signal wires used for an external circuit are the high-resistance wires.

FIG. 36 shows a portable radio equipment which is

characterized in that a part of the circumference of the housing 102 is enclosed by a ferromagnetic material 111 such as a ferrite ring or the like.

FIG. 37 shows an arrangement for constructing the portable radio equipment in which the ferromagnetic material 111 is attached around a part of the circumference of the housing 102 shown in FIG. 36. FIG. 38 shows an example of a portable radio equipment where the current distribution on the housing can be switched by an electrical switch. FIG. 39 shows a specific construction for the electrical switch 122.

FIG. 40 shows another example of the electrical switch 122 where the resistor 125 shown in FIG. 39 is replaced with the high-resistance wire 109.

FIG. 41 shows still another example utilizing the electrical switch 122 where there is provided the radio-frequency cable 127 with length thereof being an integral multiple of $\lambda/4$.

FIG. 42 shows an arrangement of the electrical switch 122.

FIG. 43 shows a typical portable radio equipment in practical use equipped with a display 320, a speaker 314, a microphone 313, a numeric key pad 320 and so on.

FIG. 44 shows a portable radio equipment with a double construction where there are provided an inner electromagnetic shield without the notch and an outer electromagnetic shield having notch 101.

FIG. 45 shows a detailed example for the seventh embodiment shown in FIG. 44.

FIG. 46 shows a cross section of the junction of the metal bodies 301 and 302.

FIGS. 47A and 47B show a development illustrating double shields.

FIG. 48 shows an enlarge view of the antenna and the vicinity of high-frequency portion shown in FIG. 45.

FIG. 49 shows a portable radio equipment having the metal body and internal circuits therein; FIG. 50 shows the portable radio equipment where the external body is wrapped with a paper board with copper foil on; FIG. 51 shows the portable radio equipment having the notch.

FIGS. 52-55 show results of the radiation pattern for the portable radios shown in FIGS. 49-51. FIG. 52 and FIG. 54 show the result for the portable radio equipment having notch therein and FIG. 53 and FIG. 55 show the result for the portable radio equipment having no notch.

FIG. 56 shows an example of the eighth embodiment using a monopole antenna which is approximately $\lambda/4$ long; a cover frame of the portable radio equipment is bent between a speaker 314 and a display 319 and the notch 101 is provided therebetween.

FIG. 57 shows a side view of the portable radio equipment shown in FIG. 56.

FIG. 58 shows a portable radio equipment having a meandering shape viewed from a side thereof. FIG. 58A shows a top view thereof; FIG. 58B shows a perspective view thereof; FIG. 58C shows a side view thereof.

FIG. 59A shows a portable radio equipment having the notch 101 where the top surface thereof is tilted and the display 319 is mounted on the tilted top surface. FIG. 59B shows a side view of the portable radio equipment shown in FIG. 59A.

FIG. 60 shows a portable radio equipment having an external input-output terminal therein where a plug 129 thereof is provided below the notch 101 and at a lower side of the housing.

FIG. 61 and FIG. 62 show still another example of the fold-type portable radio equipment having the external input-output terminal.

FIG. 63 shows a portable radio equipment where there is utilized a built-in miniature antenna such as the inverted F antenna suitable for a strong electric field and a waiting state, and there is also utilized a monopole antenna which is approximately a half-wavelength long and is pulled up for usage thereof at a weak electric field and for a communication purpose.

FIG. 64 shows a typical diversity-branch type portable radio equipment. FIG. 65 shows a diversity-branch portable radio equipment according to the tenth embodiment.

FIG. 66 shows a diversity-branch portable radio equipment where the antennas 103 and 103' are monopole antenna of quarter wavelength. FIG. 67 shows a top view of the equipment shown in FIG. 66.

FIG. 68B shows a variation, based on the embodiment shown in FIGS. 66 and 67, characterized in that there are utilized the inverted F antenna in place of the quarter-wavelength monopole antenna. FIG. 68A shows a top view of the equipment shown in FIG. 68B.

FIG. 69B shows another variation, based on the embodiment shown in FIGS. 66 and 67, characterized in that there are utilized normal-mode helical antennas. FIG. 69A shows a top view of the equipment shown in FIG. 69B.

FIG. 70 shows a portable radio equipment having retractable monopole antennas 103 and 103'. FIG. 71 shows an example of the portable radio equipment combining the notch 101 and the internal circuits.

FIG. 72 shows another example of the portable radio equipment combining the notch 101 and the internal circuits.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Features of the present invention will become ap-

parent in the course of the following description of exemplary embodiments which are given for illustration of the invention and are not intended to be limiting thereof. Embodiments of the present invention will now be described with reference to the drawings.

Embodiment No. 1

FIG. 6 shows a portable radio equipment according to the first embodiment for the present invention. In the same figure, a transmitting unit and a receiving unit are not shown. With reference to FIG. 6, the reference numeral 102 designates a housing serving as an electric shield and the reference numeral 103 is an antenna. The reference numeral 101 indicates a notch provided in the housing 102.

FIG. 7 shows a current distribution on the portable radio, indicated with broken lines, where there is provided the notch in the housing 102. Suppose that the antenna 103 is a $1/4$ -wavelength monopole antenna ($1/4$ wavelength will be referred to as $1/4 \lambda$ hereinafter). The notch 101 is provided in the vicinity of $1/4 \lambda$ away from a feeding point of the antenna 103 (indicated with ℓ in FIG. 7), and the notch is approximately $1/4 \lambda$ long.

Thus, a length of from the top end of the antenna 103 to a left end of the notch 101 is approximately $1/2 \lambda$ in terms of measurement in electrical length. Therefore, a current distribution is one which is indicated with broken lines (a). Since the length of the notch 101 is approximately $1/4 \lambda$, the current distribution around the notch 101 shall be as indicated with broken lines (b) and (c). It is to be noted that since the respective current distributions (b) and (c) exhibit same amplitudes with opposite phase to each other, electromagnetic waves radiated from those currents are cancelled out. In other words, since there disappears a portable radio's contribution to electromagnetic wave radiation due to the notch 101, a radio-frequency current flowing through the housing attributive to the radiation can be reduced and a desired radiation pattern can be obtained by simply providing a notch in the housing.

There will be shown a simulation result of a radiation pattern in the portable radio in which there is provided the notch 101 in the housing 102.

FIG. 8 shows a model of the portable radio where there is provided the notch 101 on the housing 102, in order to perform the simulation. In this model, a length from the feeding point of the antenna 103 to the notch 101 is $1/4 \lambda$ and the notch 101 is $1/4 \lambda$ long.

FIG. 9 shows the radiation pattern obtained from the above model shown in FIG. 8. In the same figure, a coordinate system is same as in FIG. 2 and FIG. 3, and the antenna 103 is placed vertical to an x-y plane. Thus, there is shown an omnidirectional (circular) characteristic in the x-y plane. In the x-z or y-z plane including an axis of the antenna, the expected maximum radiation directions lie in an x axis of the x-z plane and in a y axis of the y-z plane. Accordingly, compared to the radiation

patterns for the conventional portable radios shown in FIG. 2, the radiation patterns for the portable radio equipment according to the present invention are improved since the effect by the radio-frequency current flowing through the housing is reduced.

In FIG. 10, FIG. 11 and FIG. 12, examples which use other antennas than the $1/4 \lambda$ monopole antenna are shown.

FIG. 10 shows a portable radio using an inverted F antenna. In the same figure, the housing 102 is connected to the inverted F antenna 103 via a short-circuit wire 106 and the feeder 107. There is provided a notch 101 of length a , the notch is away from a feeder by length ℓ (approximately $1/4 \lambda$). FIG. 11 shows a portable radio using a miniature antenna 103 placed over the top surface of the portable radio. FIG. 12 shows a portable radio using a helical antenna 103. In both FIG. 11 and FIG. 12, there are provided notches with length a and positioned at ℓ so that the distribution of the radio-frequency current flowing through the housing 102 varies to reduce its influence to the radiation pattern.

FIG. 13 shows another example of the portable radio where a range of antenna length ℓ varies from approximately $3/5 \lambda$ to $3/10 \lambda$ and the notch 101 is provided at a distance ℓ from the feed point to the notch so that the distribution of the radio-frequency current flowing through the housing 102 is changed. Thereby, the radiation characteristics of the portable radio can be improved and a gain of the antenna can be increased.

In a portable radio as shown in FIG. 14 where the antenna 103 is provided in a center of a top of the housing 102, there can be obtained the same effect where the high-frequency current distribution is changed to improve the radiation characteristics.

Next, FIGS 15 through 18 show the radiation patterns in relation to the length a of notch for a being $3/16 \lambda$, $1/5 \lambda$, $1/4 \lambda$ and $1/3 \lambda$, respectively.

Comparing those radiation patterns, with reference to FIG. 15 with the length of notch being $3/16 \lambda$, the maximum radiation direction in the y-z plane (FIG. 15C) lies in a right downward inclined direction and a left downward inclined direction, thus indicating that there is little effect by providing the notch. On the contrary, with reference to FIG. 16 with the length of notch being $1/5 \lambda$, the radiation pattern in the y-z plane (FIG. 16C) shows the same level of gain in the horizontal direction and the right downward inclined as well as the left downward inclined directions, thus indicating that there is a certain effect obtained by providing the notch. In particular, with reference to FIG. 17 and FIG. 18 with the length of notches being $1/4 \lambda$ and $1/3 \lambda$, respectively, the maximum radiation direction lies in the horizontal direction, thus indicating that there is a significant effect obtained by providing the notch. As observed above, varying the length of notch can change the radiation pattern of the portable radio. Further, there can be obtained a most desirable radiation pattern by combining the length of notch, a shape of notch, a position of notch and the

number of notch.

Now, attention is directed to the position of the notch, as compared to the length of notch as described above. Let us use a model shown in FIG. 19 where the notch is located at a distance ℓ from the feed point of the antenna, the length of antenna is 0.25λ , the width of the housing 102 is 0.4λ , and the depth of the housing 102 is 0.15λ , and the length of notch is 0.25λ . FIGS 20 through 24 show the radiation patterns in relation to the position of notch with the distance ℓ being $1/16\lambda$, $5/48\lambda$, $3/16\lambda$, $1/4\lambda$ and $5/16\lambda$, respectively.

Compared the radiation patterns shown in FIGS 20 through 24 to ones of the portable radio having no notches (FIG. 2), with reference to FIG. 20 where the notch is located at a distance ℓ of $1/16\lambda$, though the radiation characteristic is changed by providing the notch, there are some improvements and some minor deteriorations in the horizontal plane (FIG. 20B). However, with reference to FIG. 21 where the notch is located at approximately 0.1λ ($5/48\lambda$), there is only improvement and no deterioration. With reference to FIGS. 22 through 24 where the notch locations are from $5/48\lambda$ to $5/16\lambda$, there is observed no deterioration. According to the above data, if the notch is located off by more than approximately 0.1λ , there is observed a positive effect of providing a notch and the radiation pattern in the horizontal direction is improved. The above results indicate that the location of the notch can be not only at approximately $1/4\lambda$ but also at other distances to have a positive effect of having notch in the housing of the portable radio equipment. Therefore, the distance ℓ of the notch can be adjusted according to a certain condition.

Next, FIG. 25 and FIG. 26 show an example of the portable radio having a plurality of notches 101 in combination to vary the distribution of the radio-frequency current flowing through the housing 102 so that the radiation characteristics of the portable radio can be improved.

FIG. 25 shows a portable radio where there are provided two notches in the same side of the housing 102. With reference to FIG. 25, there are provided two notches of length a , b on the side close to the feed point of $\lambda/4$ antenna. Suppose that the length a , b of notches and distance ℓ from the feed point to the first notch are approximately $\lambda/4$, and distance n from the first notch to the second notch is approximately $\lambda/2$.

In the above configuration shown in FIG. 25, as have described in regard to FIG. 7, the first notch lies in a loop of the radio-frequency current and, moreover, the second notch placed at a distance of approximately $\lambda/2$ from the first notch also lies in the loop of the high-frequency, thus the radiation characteristics being further improved. It shall be appreciated that though the effects of radiation characteristics are somewhat less effective when ℓ and n are set to other than $\lambda/4$ and $\lambda/2$, respectively, the position and length of the notches can be designed freely according to a designing situation.

FIG. 26 shows an example of the portable radio

where there are provided two notches one of which is provided from a side of the housing 102 while the other notch is provided in the opposite side of the housing 102. Suppose that respective length of the notches are a and b , and a distance from the top end of the housing to the first notch 101 is indicated with ℓ and a distance from the top end of the housing to the second notch 101 is indicated with n . In this embodiment represented by FIG. 26, by providing the two notches at a relatively close distance therebetween and providing one notch from one side and other from the opposite side, the radio-frequency current can be concentrated around the two notches.

In the above embodiment represented by FIG. 26, the distribution of radio-frequency current is localized in a concentrated area, moreover, there are provided two notches at an opposite direction to each other so that phases of the radio frequency can be made to coincide. A significant effect can be obtained when length a , b is approximately $\lambda/4$, and distance ℓ is approximately $\lambda/4$ and distance n is designed to be longer than ℓ .

Embodiment No. 2

FIG. 27 and FIG. 28 show portable radio equipment having different types of notches 101.

FIG. 27 shows a portable radio equipment having an L-shaped notch 151. In the same figure, let respective length of the notch 151 be a for a horizontal line and b for a vertical line as shown in the figure. In this embodiment, the length of the notch 151 is adjusted such that $(a + b)$ equals to approximately $\lambda/4$.

FIG. 28 shows a portable radio equipment having a T-shaped notch 153. In the same figure, let respective length of the notch 153 be c for a horizontal line and d for a vertical line as shown in the figure. In this embodiment, the length of the notch 153 is adjusted such that $(c + d)$ equals to approximately $\lambda/4$.

In above embodiments as shown in FIG. 27 and FIG. 18, length ℓ from the feeding point of the antenna 103 is set to approximately $\lambda/4$ and the total length of the notch is set to approximately $\lambda/4$, in other words, a total circumference of the notch that equals to $(a + b + b + a)$ is set to approximately $\lambda/2$, so that the same effect can be obtained as set forth as in FIG. 6. The embodiments represented by FIG. 27 and FIG. 28 can be useful when size of a conductive body, i.e. housing, is relatively small.

FIG. 29 illustrates directions of the current flowing around the notch. FIG. 29A shows directions of the current flowing around an I-shaped notch. FIG. 29B shows directions of the current flowing around the L-shaped notch. FIG. 29C shows directions of the current flowing around the T-shaped notch.

With reference to FIG. 29A through FIG. 29C, the currents flowing along the notch are considered that the current flowing along an upper side of the notch is opposite in direction and same in amplitude to the current

flowing along a lower side of the notch so that the currents are cancelled out, thus not contributing affects thereof to the radiation. Therefore, by providing such notches as illustrated in FIG. 29, it is possible to minimize the affect of the radio-frequency flowing through the housing 102 on the radiation pattern. When the width of the portable radio equipment is shorter than $\lambda/4$, it is difficult to provide the I-shaped notch in the housing 102. In that case, the L-shaped and T-shaped notches will be useful. In other words, when the width of the portable radio equipment is less than $\lambda/4$ and it is physically difficult or impossible to provide a notch due to a restriction caused by arrangement of internal units of the housing such as a transmitting unit or a receiving unit, a degree of freedom in terms of designing a notch as well as the portable radio equipment as a whole is increased by adopting an L-shaped or T-shaped notch as illustrated in FIG. 29.

FIG. 30 and FIG. 31 show another embodiment in providing a notch to the housing 102.

FIG. 30 shows a portable radio equipment having a longitudinally tilted notch 155. FIG. 31 shows a portable radio equipment having a smoothly curved notch 157. By providing the tilted notch and curved notch to the housing 102 as illustrated in FIG. 30 and FIG. 31, there can be obtained the same effect as in FIG. 6. In other words, by providing such notches as in FIG. 30 and FIG. 31, the distribution of current flowing through the housing is altered so as to reduce the affect thereof on the radiation pattern.

Embodiment No. 3

FIG. 32 shows a portable radio equipment having a notch 101 where there is provided a coil 104 or a ferrite ring 105 in the notch 101 so as not to short-circuit the notch. A self-inductance value for such elements as the coil 104 and the ferrite ring 105 are preferably at least a few μH so that a desired length for the notch can be secured.

In the present invention, there is provided means for changing the current distribution on the housing so as to change the current distribution of the radio frequency and thereby improve the radiation characteristic of the whole portable radio equipment. Therefore, since the less the radio-frequency current is generated on the housing the less the electromagnetic wave is radiated, the longer the width of the notch 101 becomes the greater the improvement on the radiation characteristic becomes.

In the third embodiment, strength in the whole portable radio equipment can be secured by inserting, between the notch, a dielectric such as a glass epoxy FRP, a Teflon base plate or a usual plastic so as to fix the housings, thereby obtaining the same effect as described before.

There is shown another example for the third embodiment in FIG. 33. FIG. 33 shows a portable radio

equipment having a notch 101 where there is provided an optical fiber 204 for communicating a signal between an upper portion of the housing and a lower portion of the housing. In this embodiment, the notch 101 is provided at a distance of approximately $\lambda/4$ from a top end of the housing and the length of the notch 101 is approximately $\lambda/4$ long. The shape of the housing 102 is arbitrary to a certain degree. The antenna 103 is set on either end of a longitudinal side of the housing 102. In FIG. 33, the reference numerals 201 and 202 show internal circuits, for example, 201 for a transmitting or receiving circuit and 202 for a control circuit, a synthesizer or a receiving or transmitting circuit.

In this embodiment represented by FIG. 33, the embodiment is characterized in that there is provided the optical fiber 204 for communicating the signal between an upper portion and a lower portion of the notch via the optical fiber 204 which is non-conductive. In other words, the transmitting/receiving circuit 201 and the control circuit 202 are connected via an electric signal wire 108 through which an electric signal is inputted and outputted. The electric signal communicated through the electric signal wire 108 is converted to an optical signal by a photoelectrical transfer unit 203, and thereafter the optical signal is transferred through the optical fiber 204 bridging between the notch 101, and then the optical signal is converted to an electric signal by a photoelectrical transfer unit 203 so that the signal is transferred through the electric signal wire.

Accordingly, by employing the nonconductive material for the signal wire crossing through the notch 101, an electromagnetic radiation can be prevented and the communication of signals between the notch 101 can be performed without a loss of the effect of having the notch 101. With reference to FIG. 33, the internal circuits 201 and 202 are, for instance, circuits such as a control circuit or the like which deal with a signal of relatively low frequency. An external circuit 110 is for a key pad or a display (see FIG. 35). FIG. 34 shows a portable radio equipment utilizing a high resistance wire 109 in place of the optical fiber 204 shown in FIG. 33.

With reference to FIG. 34, the reference numeral 201 designates a receiving circuit, 202 a transmitting circuit, 113 an antenna shared device, 114 a synthesizer, 115 a control circuit and 116 is a power source. The reference numeral 117 indicates a radio-frequency cable for transferring the radio-frequency signal. There is provided the signal wires from the control circuit 115 to the transmitting circuit 202, and among such signal wires the high-resistance wire is utilized for a portion crossing the notch 101 and for the rest of area there are used cables for baseband digital or analog signal. In this embodiment represented by FIG. 34, the transmitting circuit 202 and the receiving circuit are separately disposed in the upper portion and the lower portion of the housing, respectively, so that the number of type of the signal to be transferred through the notch 101 can be reduced and the number of the signal wires can also be

reduced.

FIG. 35 shows a portable radio equipment where whole signal wires used for an external circuit 110 are the high-resistance wires 109. In particularly the external circuit 110, there exists a great influence of the electromagnetic wave radiated from the current flowing through the signal wire. Therefore, by replacing the signal wires (for connecting the external circuits disposed in the upper and lower portion of the notch 101) by the high-resistance wires, the influence of the electromagnetic wave upon the radiation characteristic can be reduced.

Embodiment No. 4

FIG. 36 shows a portable radio equipment which is characterized in that a part of the circumference of the housing 102 is enclosed by a ferromagnetic material 111 such as a ferrite ring or the like. Since in general the ferromagnetic material 111 presents a high resistance in a high-frequency area, the distribution of the radio-frequency current flowing through the housing 102 can be changed by enclosing the part of the housing 102 with the ferromagnetic material. Differing from the embodiments where the housing has the notch therein, the distribution of the radio-frequency current flowing through the housing 102 can be changed without deforming the housing in any way. Therefore, the electric wave radiation characteristic can be improved without deforming or rearranging base plates, circuit parts or signal wires and so on already provided in the housing.

FIG. 37 shows an arrangement for constructing the portable radio equipment in which the ferromagnetic material 111 is attached around a part of the circumference of the housing 102 shown in FIG. 36. With reference to FIG. 37, a ferrite 111a (□-shaped portion indicated with hatched lines) and a ferrite 111b are provided in a □-shaped portion of the housing 102-a and the housing 102-b, respectively. Anything may be suitable if the housing is of conductive nature. The housing may be such that a dielectric such as a plastic serving as an outer frame is provided where in an inner surface of the outer frame there may be provided a conductive thin film and conductive coating or the like. The housing 102a and 102b are arranged so that the ferrite 111a and the ferrite 111b do not contact with the housing 102a and 102b, respectively. Metals 112a and 112b combined are arranged to be electrically contacted to an outside of the □-shaped portion of the housings 112-a and 112-b so that an inside of a ring constituted by combining the ferrites 111a and 111b is electromagnetically shielded. Accordingly, there is provided an electromagnetic shield against the outside of the housing 102 and the inside of the ferrite ring, and a high-frequency signal component tending to penetrate the ferrite ring can be shielded.

Embodiment 5

The present invention is characterized in that the radiation pattern of the electromagnetic wave is improved by providing the notch in the housing. In addition to the feature of the present invention characterized in having the notch in the housing, it is possible to have a diversity function by switching the distribution of the radio-frequency current flowing through the housing so as to change the radiation pattern of the electromagnetic wave.

FIG. 38 shows an example of a portable radio equipment where the current distribution on the housing can be switched by an electrical switch. In this embodiment, the electric wave which arrives at the portable radio equipment is received by the antenna 103, and a signal S1 received by the antenna 103 is fed to a receiving circuit 104 and an evaluation circuit 120. In the evaluation circuit 120, an error rate of an input signal S1 is detected and a transmitting and receiving state is evaluated. For example, when a time-division multiplex access is utilized for a communication system, evaluation is carried out using the input signal S1 during a time zone of no transmitting or receiving in your own portable radio equipment after confirming by an input signal S2 that a radio terminal in use by yourself is not transmitting or receiving. In such manner as mentioned above, a disturbance against the transmission and receive due to a noise generated at the time of switching can be eliminated without information being interrupted during communication.

The evaluation circuit 120 sends out an evaluation signal S3 to a switch driver 121 in terms of a signal strength of the input signal S1. The evaluation signal S3 is given on the basis of, say, a voltage, current and so on. In the switch driver 121, sent to the electrical switch 122 is a control signal S4 which instructs the electrical switch 122 to close or open the electrical switch 122 based on the evaluation signal S3 sent from the evaluation circuit 120. Upon receipt of the control signal S4, the radio-frequency electrical switch 122 provided in the proximity of an open end of the notch 101 switches over between a short-circuit and open of the open end of the notch 101.

In a practical use, a diversity system of the radio terminal is first operated at a test mode of transmission or receive. Namely, after confirming by the signal S2 that the portable radio equipment of your own is not transmitting or receiving, the evaluation circuit 120 sends out to the switch driver 121 a signal instructing make and break of the electrical switch 122 at a predetermined interval, and the respective input signals S1 when the electrical switch 122 is opened and the electrical switch 122 is short-circuited are stored as data in a memory within the evaluation circuit 120. For the two states, respective error rates of the input signals are detected and compared so as to evaluate which one is a better transmitting/receiving state.

One whose receiving state is better is chosen based on an evaluation result, and the electrical switch 122 is chosen so as to keep such a state. Then S3 is sent out to the switch driver 121 instructing to send to the electrical switch 122 and hold the signal S4 indicating the chosen state.

Accordingly, after operating at the test mode, the evaluation circuit becomes an evaluation mode for evaluating S1 for a predetermined duration of time and at a predetermined interval. Only when a transfer quality of the input signal S1 is inferior to a predetermined state, the radio terminal becomes the test mode again. It shall be appreciated that the transfer quality may be examined routinely after the predetermined duration of time elapses.

Even when the information quality deteriorates, switching the high-frequency electrical switch 122 makes possible that the portable radio equipment terminal is used with the radiation pattern being switched in accordance with the quality.

FIG. 39 shows a specific construction for the electrical switch 122. FIG. 39 shows an enlarged view of the notch 101 provided in the housing 102. With reference to FIG. 39, a diode 123 is connected to an end of an open end- of the notch 102-a. A resistor 125 and a capacitor 124 are connected in parallel to the diode 123. The other end of the resistor 125 is connected to a controlled potential 126 and the other end of the capacitor 124 is connected to the other end of the open end of the notch 102-b.

When a direct current flows through the electrical switch 122, a resistance value of the diode 123 is decreased, so that the radio-frequency current flows and the open end 102-a of the notch 101 is short-circuited to the other open end 102-b of the notch 101 through the capacitor 124. Moreover, the capacitor 124 prevents the direct current from flowing to the housing 102, and the capacitor 124 operates to be short-circuited against the radio-frequency current. Assuming that a voltage of the controlled potential is at a level of approximately 5 V, a value of the resistor 125 may be approximately 1 K Ω and a value of the capacitor 124 may be approximately 10 pF.

FIG. 40 shows another example of the electrical switch 122 where the resistor 125 shown in FIG. 39 is replaced with the high-resistance wire 109.

FIG. 41 shows still another example utilizing the electrical switch 122 where there is provided the high-frequency cable 127 with length thereof being an integral multiple of $\lambda/4$. An inner conductor of the high-frequency cable is placed close to an open end 102-a of the notch 101, and an outer conductor of the high-frequency cable 127 is grounded at a corresponding point in the open end 102-b of the notch 101.

By this configuration illustrated in FIG 41, the operation of the electrical switch 122 can be changed according to the length of the high-frequency cable 127. Namely, when the length of the high-frequency cable

127 equals to an odd-integral multiple of quarter wavelength of the frequency used for transmission or receive, the notch 101 is opened when the electrical switch 122 is short-circuited whereas the notch 101 is circled when the electrical switch 122 is opened. When the length of the high-frequency cable 127 equals to an even-integral multiple of quarter wavelength of the frequency used for transmission or receive, the notch 101 is short-circuited when the electrical switch 122 is short-circuited while the notch 101 is opened when the electrical switch 122 is opened. As far as the electrical switch 122 is located in the vicinity of the open end of the notch 101, an effect thereof can be maintained.

FIG. 42 shows an arrangement of the electrical switch 122. When the electrical switch is relatively a large-sized, a part of the notch 101 may be extended in a vertical direction as illustrated in FIG. 42 so that the electrical switch 122 can be positioned within the notch 101. However, even though the electrical switch 122 is not fit perfectly within the notch 101, the operation of the electrical switch 122 may not be affected.

Embodiment No. 6

There have been shown the portable radio equipment having the notch or notches therein in order to alter the radio-frequency current distribution and improve the radiation pattern of the electric wave.

However, the portable radio equipment in practical use must be equipped with a display 320, a speaker 314, a microphone 313, a numeric key pad 320 and so on as shown in FIG. 43. The display 320 and the numeric keys 320 particularly require relatively many set of signal wires. Thus, when the notch 101 is covered with such signal wires, there may be a case where it is rather difficult to alter the distribution of the radio-frequency current by providing the notch 101 alone. However, taking action to avoid such inconvenience may result in a complicated and time-consuming task. Moreover, besides a problem of the signal wires, that such components as the display 320, speaker 314, microphone 313, numeric keys 320 and so on may cover the notch 101 may significantly reduce the effect of the notch 101.

In order to solve such problems, there are provided means for shielding the electromagnetic wave by means of a double construction which is electrically insulated and wherein the notch is not provided in the inner electromagnetic shield while there is the notch in the outer electromagnetic shield, in this sixth embodiment.

FIG. 44 shows a portable radio equipment with a double construction where there are provided an inner electromagnetic shield without the notch and an outer electromagnetic shield having notch 101. In the same figure, there are provided a metal body 102-a and a metal body 102-b so as to form the double construction. There is provided the notch 101 in the outer metal body 102-a. It shall be appreciated that the metal bodies 102-a, 102-b can be anything having a shielding effect,

for example, there can be considered metal with conductive coating and plating (aluminum plating, nickel plating, etc), copper, aluminum and so on, or material combined. A bag-like thing made of a metal thin film may be utilized as the inner metal body 102-b, and a plastic frame or the like may be utilized as the outer metal body 102-a.

FIG. 45 shows a detailed example for the sixth embodiment shown in FIG. 44. With reference to FIG. 44, an internal circuit board 304 is enclosed by the metal body 301 and 302. In the circuit board 304, there are mounted a transmitting portion 305 and a receiving portion 306, a control circuit, low-frequency circuit, a power supply portion 307 and a feed portion to the antenna. The notch 101 is provided in the metal body 301, 302. The metal body 302 may be such that, for instance, the conductive coating is applied to a frame formed by a plastic and thereon the nickel is plated. The notch 101 can be formed by masking on the plastic frame when applying the conductive coating. The notch 101 can be formed in the metal body 301 in the same manner. No plating is performed on mounting portions for a connector, the antenna, the microphone and so on. The conductive coating is applied to a hole for the feed portion of the antenna 103. Accordingly, the plated conductive portions in the metal bodies 301, 302 are electrically insulated in non-conductive coated portions of junction of the metal bodies 301, 302.

FIG. 46 shows a cross section of the junction of the metal bodies 301 and 302. The inner part and outer part of the metal body which is constructed by the metal bodies 301 and 302 are covered with conductive members such as plating, and the these conductive members are electrically insulated. Therefore, the metal bodies 301 and 302 must be connected so that the inner part and the outer part thereof remain insulated to each other (see FIG. 47).

With reference to FIG. 45, on the body 301 there is provided a board 321 in which the display 319 and an electrical line of a key pad 320 are mounted. The board 321 is arranged so as not to interfere with the effect realized by the notch 101 and in a manner that the board 321 is not overlapped with the position of the notch 101. In a similar way, the speaker 314 is mounted to the body 301 so that the speaker 314 is not overlapped with the position of the notch 111.

There are provided some holes in the body 301, so that connectors connecting the board 321 and a control circuit 307 and jacks 37 connecting external plugs such as an earphone and a head set can be connected to the control portion 307. In particular, the antenna 103 is also connected to a feed point through a hole provided in the body 301.

In this embodiment, there is used a $\lambda/4$ monopole antenna of a spring-type device having a very thin radius. The antenna is fixed on the conductive body by the connector 323. The reference numeral 311 indicates an antenna connector.

The reference numeral 325 and 315 construct a battery box, and the conductive member such as plating is applied up to and point of the notch 101 so as to be electrically shielded. The battery box is connected to the bodies 301, 302 through a power connector 308. The bodies 301 and 302 are covered with a plastic body 312 and a battery box panel 325 so as to constitute a portable radio equipment.

FIG. 48 shows an enlarge view of the antenna and the vicinity of high-frequency portion in the sixth embodiment shown in FIG. 45.

A ground terminal 332 of an antenna duplexer or switch 307 is short-circuited to a ground 326 of the board, and a circuit 367 in the vicinity of the antenna 103 and the antenna duplexer or switch 307 is enclosed by the metal body 302 mounted on the back of a ground 326, the metal body 301 and the board 304 so as to be shielded. The board 304 is a multiple layer type board, and in order to increase the shield effect of the board there are provided through holes around the ground 326.

A transmit terminal 328 and a receive terminal 327 of the antenna duplexer or switch 307 are connected to a transmitting portion 305 and a receiving portion 306, respectively, through terminals 360, 361 on the board and wires on a board below the ground 326. Other wires used for other control pass through these through holes. It is to be noted that when an interval is set to a distance sufficiently smaller than the wavelength, there will be caused no influence over the shielding effect. The ground 326 has contact with an internal conductor of the metal body 302 but does not have contact with an external conductor of the metal body 302. The antenna 103 is connected to an antenna terminal 327 of the antenna shared device 307 through a matching circuit 330 for the antenna and feeder.

FIG. 47 shows a detailed figure to show the bodies according to the above sixth embodiment.

The bodies 301 and 302 are made of dielectric such as a plastic, and an electric conductive material is fixed, applied or plated on a surface thereof so as to serve as an electromagnetic shield. Especially in this sixth-embodiment, the electromagnetic shield is provided in double construction so as to improve the radiation pattern effectively. In the double construction of the electromagnetic shield, a conductive portion in each double shield is not electrically connected to each other. A portion a and portion a' shown in the cross section and a notch portion, that are, portion shown with no hatching in the figure are such that plating is not performed by means of a masking or the like.

The body 302 is designed to be inserted to the body 301, and when inserted the body 302 is divided into an internal plating portion and a notch-made external plating portion by the portion a and the portion a' in terms of the high frequency; the plating is carried out in a manner that the internal portion comes in contact with the external portion in a portion where the antenna is insert-

ed. The notches 101 are made on the body 301 and the body 302 so that the notches are combined together when inserted.

In this sixth embodiment, the electrical insulation between the internal conductor and the external conductor is not absolutely necessary, and a part thereof may be electrically contacted as will be described below.

FIGS 49-51 show a model, used in an experiment carried out by the applicants, where there is provided the notch in the metal body containing the metal body having radio circuits therein. FIG. 49 shows a portable radio equipment having the metal body and internal circuits therein; FIG. 50 shows the portable radio equipment where the external body is wrapped with a paper board with copper foil on; FIG. 51 shows the portable radio equipment having the notch. Assume that there is no radio-frequency point between the external body and the internal body.

FIGS. 52-55 show results of the radiation pattern for the portable radios shown in FIGS. 49-51. FIG. 52 and FIG. 54 show the result for the portable radio equipment having notch therein and FIG. 53 and FIG. 55 show the result for the portable radio equipment having no notch. Observing the results, the maximum directional gain comes closer to the horizontal direction. Accordingly, it is observed that the radiation pattern can be improved by providing the notch and without changing the internal circuits at all. It shall be appreciated that even though the external conductor comes in contact with the internal conductor at an antenna feed portion, radiation from the internal metal body is reduced on account of Faraday effect and there can be obtained the effect of having the notch in the external body.

FIG. 71 shows an example of the portable radio equipment combining the notch 101 and the internal circuits. The notch 101 is provided just below the speaker 314 in which there are relatively fewer signal wires as compared to the display 319 and the switch 320 for the numeric keys. The signal wires are gathered together to be guided into the conductive body by way of a connector 318.

FIG. 72 shows another example of the portable radio equipment combining the notch 101 and the internal circuits. The signal wires for the display 319 and the numeric keys switch 320 are guided into the conductive body in the vicinity thereof by way of respective connectors thereof 318. The notch 101 is provided between the display 319 and the numeric keys switch 320.

Embodiment No. 7

In the future, there will be an occasion that the portable radio equipment is so compact-sized and often-times is placed and carried in a chest pocket. However, the portable radio equipment is susceptible to a human body and thus a radiation characteristic of the equipment fluctuates significantly. It is already known by a study result carried out by the inventors of the present

invention that a radiation efficiency of an electric-field antenna decreases when the antenna approaches to the human body. Thus, there is a problem where the radiation characteristic deteriorates due to an influence of the human body when the portable radio equipment is carried in the chest pocket or the like.

Though the antenna is designed to be placed further away from the human body, the antenna may accidentally faces up closer to the human body instead as far as the portable radio equipment is placed in the chest pocket. In this connection, a direction of the antenna need be kept in a determined direction. However, it is not realistic to force a user to put the portable radio equipment in one fixed direction every time the equipment is put in the chest pocket of the user. Moreover, when the portable radio equipment becomes more and more compact-sized the antenna approaches ever close to the head of the human body. In this case, it is already confirmed by the inventors of the present invention that the radiation characteristic of the equipment is greatly influenced by the human body.

When communicating information using the portable radio equipment having a display thereon, conventionally the display is often located near a center of the equipment so that the portable radio equipment must be taken out of the chest pocket to see the display. To alleviate such troublesome action, there are considered the following embodiments.

FIGS. 56 and 57 show an example of the seventh embodiment using a monopole antenna which is approximately $\lambda/4$ long. A cover frame of the portable radio equipment is bent as illustrated in the figure between a speaker 314 and the display 319 and the notch 101 is provided therebetween. As shown in FIG. 57, an angle bent θ is for example an approximately 30 degrees from the vertical line. The antenna 103 is mounted on top of the housing along the same bent direction with the display 319 mounted on the conductive body. The antenna 103 is covered with an elastic dielectric such as vinyl radome and an element in the monopole antenna is made of a very thin spring or wire whose diameter is, say, approximately $\lambda/100$. A distance between a transmitting unit and a receiving unit is approximately 15 cm though the distance shall vary depending on a shape of the portable radio equipment.

FIG. 58 shows a portable radio equipment having the notch 101 and a meandering shape viewed from a side thereof. FIG. 58A shows a top view thereof; FIG. 58B shows a perspective view thereof; FIG. 58C shows a side view thereof. The antenna 103 may be an inverted F antenna for instance. The antenna 103 can be made of a conductor wire whose diameter is approximately $1/100$ of antenna diameter, or can be made by constructing a strip line on the dielectric board by means of etching or the like.

FIG. 59A shows a portable radio equipment having the notch 101 where the top surface thereof is tilted and the display 319 is mounted on the tilted top surface. FIG.

59B shows a side view of the portable radio equipment shown in FIG. 59A. The antenna 103 utilizes, for instance, a helical antenna covered with the radome and is disposed parallel to a longitudinal axis of the housing.

Embodiment No. 8

There is a case where an external input-output terminal such as a earphone terminal, an external power terminal and an external microphone terminal is provided on the body of the portable radio equipment. When an external system is connected to the terminal, it is confirmed by the inventors of the present invention that the radiation characteristic deteriorates since the radio-frequency current flows through the external system.

In order to solve such a problem, the following configuration is considered.

FIG. 60 shows a portable radio equipment having an external input-output terminal therein where a plug 129 of the earphone and headphone or the like is provided below the notch 101 and at a lower side of the housing if the longitudinal direction of the equipment is held vertically. When there are provided a transmitting piece and a receiving piece on the portable radio equipment body, a jack 130 which is plugged in the plug 129 not only sends the transmit-receive signal but also serves as a switch by which the signal to the transmitting-receiving pieces mounted on the portable radio equipment body can be cut off.

FIG. 61 and FIG. 62 show still another example of the fold-type portable radio equipment having the external input-output terminal. The jack 129 is provided in an opposite side of the body having the notch 101 against the antenna 103, regardless of the folded or open positions. If the notch 101 is provided in an upper-half portion of the fold-type portable radio equipment and a second notch is not provided in a corresponding lower-half portion, the radio-frequency current may be distributed over the corresponding portion in the lower-half portion of the housing so that the radiation pattern unwantedly fluctuates. Thus, by providing such notch 101 in the lower-half portion too as in FIG. 63B, such a problem can be solved when the fold-type portable radio equipment is in a folded position. Then, the communication is carried out using the earphone or microphone 313.

Embodiment No. 9

FIG. 63 shows a portable radio equipment where there is utilized a built-in compact (miniature) antenna such as the inverted F antenna suitable for a strong electric field and a waiting state, and there is also utilized a monopole antenna which is approximately a half-wavelength long and is pulled up for usage thereof at a weak electric field and for a communication purpose. In this case, a direction of the minimum directional gain is known to be directed downwardly, thus causing a problem considering the fact that the electric wave generally

arrives from a horizontal direction.

A diversity antenna branch in current use is such that one is the monopole antenna which is approximately quarter-wavelength long and the other is the inverted F antenna, as shown in FIG. 63. In this case, each operational gain between the two antenna differs from the other's, so that even if a correlation factor between the antennas is low a high diversity gain can not be obtained.

In conventionally diversity-branch portable radio equipment, the two small antennas are disposed at quite a distance from each other, as shown in FIG. 64. This is because the radiation from the conductive body is relatively large when the small antenna is utilized and thus the correlation factor for the antenna does not come down and because influence by the human body is greater compared to the half-wavelength monopole antenna. In view of the foregoing problem, there can be considered that the radiation pattern can be changed so as to realize the diversity function by means of interaction between the two antennas caused by locating the monopole antenna closer to the other antenna. However, in this case, an impedance thereof is changed due to the interaction between the antennas, so that a matching circuit will be required to solve such an extra problem, thus being an unrealistic solution.

In an antenna-switching diversity in the conventional portable radio equipment, a plurality of antennas are provided in the close proximity, so that mutual impedance must be taken into consideration since interaction between the antennas is not negligible. Therefore, though there has been a suggestion that a matching circuit shall be mounted at the feed point, it is very difficult to have an identical radiation efficiency among respective antennas so as to obtain a high diversity gain, since various types of antenna are often used to construct the diversity branch so that the influence of the human body against respective different antennas differs by each antenna and a matching loss for the antenna and feeder also differs by each antenna. To make the problem worse, a value of the matching circuit must be changed in terms of a conductor loss of the matching circuit and the influence of the human body.

In view of the above drawbacks, with reference to FIG. 66, there is provided a portable radio equipment having the notch 191 therein with a plurality of antennas.

In FIG. 65, there are provided an antenna 103 and an antenna 103' disposed next to the antenna 103 both of which are mounted on the top surface of the housing 102. By providing the notch 101 on the side of the body 102 close to the antenna 103, the radio-frequency current flowing from the notch to the bottom on this side is reduced. As a result, an electromagnetic radiation from the conducting body decreases. In other side of the body 102 in the vicinity of the antenna 103, by not providing the notch on this side there is distributed a radio-frequency current from the top of the conducting body to the bottom, and the radiation of the antenna is affected

by the current, thus the radiation thereof being significantly present indicating that the effect of providing the notch is rarely present. Knowing accordingly, a proper use can be realized between a diversity of the antennas and a plurality of antennas, so that the radiation pattern can be freely changed.

FIG. 66 shows a diversity-branch portable radio equipment where the antennas 103 and 103' are monopole antenna of quarter wavelength. The reason for selecting such length is because the current flowing through the conductive body mounting the antennas with such length is relatively large and the provision of the notch plays an important role. Accordingly, since the correlation factor of the antenna is small and the maximum actual gains thereof are substantially equal, the diversity antenna branch can be constructed having an increased diversity gain. The each antenna may be arranged in a position so that the interaction between the antennas remains weak. The antennas 103 and 103' may be mounted in a different side of the conductive body from one where the transmitting or receiving pieces are mounted, so that the influence caused by subjecting the equipment to the head of the human body can be minimized. Moreover, the diversity method may be applied such that the equipment becomes a diversity after detecting the electric wave, thus improving practicality of this ninth embodiment. Moreover, in the similar manner, the circuit required for a radio portion can be merely one circuit, thus realizing in further compactness of the equipment.

FIG. 68 shows a variation, based on the embodiment shown FIG. 66, characterized in that there are utilized the inverted F antenna in place of the quarter-wavelength monopole antenna. Since the current flowing through the conductive body is considered to be large, the notch plays an important role. Moreover, the tips of the antennas 103 and 103' may be bent so as to economize a space required for the antennas and to reduce interaction therebetween by avoiding being too close to each other. This embodiment is suitable for realizing the built-in antennas since height of the antennas is made comparatively short.

FIG. 69 shows another variation, based on the embodiment shown in FIG. 66, characterized in that there are utilized normal-mode helical antennas. In the portable radio equipment according to the embodiment shown in FIG. 69, the antennas can be made compact-sized and can be placed away from the human body.

FIG. 70 shows a portable radio equipment having retractable half-wavelength antenna 103 and an inverted F antenna. A half-wavelength monopole antenna on the conducting body radiates a close field of the half-wavelength dipole antenna, since the current flowing on the conducting body is less than that of a quarter-monopole antenna. However, the radiation from the inverted-F antenna is affected by the current on the conducting body as in the case of the quarter-wavelength monopole antenna. Therefore, the gain of the inverted-

F antenna is weaker than that of the half-wavelength monopole antenna in the absence of a notch on the conducting body. By providing the notch on the conducting body at a side near the inverted-F antenna, an undesirable current on the conducting body is reduced and the difference of the gains between two types of antennas are minimized. The equipment represented by FIG. 70 is used for a telephonic communication since there is caused less influence from the head of the human body as compared to the built-in type antennas. The antenna 103' is the inverted F antenna which is suitable and utilized for a waiting state. It shall be appreciated that there may be provided an electrical switch for automatically switching the feed circuit from the antenna 103 to the inverted F antenna 103' when the antenna 103 is pushed down to be contracted.

The antenna to be used for the above all embodiments may be the monopole type antenna, the inverted F antenna, the normal-mode helical antenna or other antennas used widely for the portable radio equipment. The present invention can also be applied to other radio equipment including a housing serving as electromagnetic shield, an antenna attached to the housing and transmit-receive circuits therein such as radio-type card, radio-type personal computer, radio LAN, various compact radio base station.

As described above, by employing the present invention, the influence of the radio-frequency currents flowing through the shield means can be minimized, thus improving significantly the radiation pattern of the portable radio equipment.

Besides those already mentioned above, many modifications and variations of the above embodiments may be made without departing from the novel and advantageous features of the present invention.

Claims

1. Portable radio equipment provided with an antenna (103) for transmitting and receiving electromagnetic waves, a housing (102) on which the antenna is mounted and having a notch (101) therein, said housing being made of an electromagnetic shielding material, and an internal circuit connected to the antenna (103) for generating and receiving the electromagnetic waves through the antenna (103), characterized in that the notch (101) is arranged in the housing (102) in a manner to modify the radiation pattern caused by radio frequency currents flowing on the housing (102).
2. The portable radio equipment according to claim 1, wherein the antenna (103) is an inverted F type miniature antenna (103) disposed on the housing (102).
3. The portable radio equipment according to claim 1,

- wherein the antenna (103) is a miniature type antenna (103) disposed over a top of the housing (102).
4. The portable radio equipment according to any preceding claim, wherein the antenna (103) is approximately quarter wavelength long and the notch (101) is disposed at a distance of approximately quarter wavelength from a top end of the housing (102).
 5. The portable radio equipment according to any preceding claim, wherein the notch (101) is approximately quarter wavelength long.
 6. The portable radio equipment according to any preceding claim, wherein a plurality of notches (101) are disposed in the housing (102).
 7. The portable radio equipment according to any preceding claim, wherein the internal circuit includes a first circuit (202) for transmitting the electromagnetic wave and a second circuit (201) for receiving the electromagnetic wave, and the first circuit is disposed in an upper portion of the notch in a case where the second circuit is disposed in a lower portion of the notch (Figs. 33-34).
 8. The portable radio equipment according to any preceding claim, wherein ferromagnetic material (111) is attached around a part of the circumference of the housing (102).
 9. The portable radio equipment according to any preceding claim, wherein the housing (102) includes receiving means (104) connected to the antenna (103) for receiving one electromagnetic wave (S1) from the antenna (103) and outputting a signal (S2) when the antenna (103) does not receive another electromagnetic wave and does not transmit the electromagnetic wave, evaluation means (120) connected to the antenna (103) and the receiving means (104) for detecting an error rate of the one electromagnetic wave (S1) supplied from the antenna (103) and outputting an evaluation signal (S3) on the basis of the detected one electromagnetic wave when receiving the signal (S2) from the receiving means (104), switch driver means (121) connected to the evaluation means (120) for receiving the evaluation signal (S3) from the evaluation means (120) and outputting a control signal (S4) based on the received evaluation signal (S3), and switch means (122) disposed in the vicinity of an open end of the notch (101) and connected to the switch driver means (121) for electrically opening and short-circuiting the open end of the notch (101) in response to the control signal (S4) supplied from the switch driver means (121) (Fig. 38).
 10. The portable radio equipment according to any preceding claim, wherein the housing (102) has an internal conductive shield thereinside (Fig. 37).
 11. The portable radio equipment according to claim 10, wherein the internal conductive shield includes an internal body (102-b) and an external body (102-a) having the notch therein, the internal body (102-b) and the external body (102-a) are made of electric conductive material and include conductive coating and plating such as aluminum plating and nickel plating, copper, aluminum, or material combined thereof, and the internal body (102-b) and the external body (102-a) are insulated to each other (Figs. 37, 39, 41).
 12. The portable radio equipment according to claim 10, wherein the housing (102) further has a nonconductive frame body disposed on the internal conductive shield.
 13. The portable radio equipment according to any preceding claim, wherein a plurality of monopole antennas being quarter wavelength long are mounted on the housing (102).
 14. The portable radio equipment according to claim 13, wherein a plurality of converted F antennas or helical antennas, or in combination, are disposed on the housing (102) so as to constitute a diversity branch.
 15. The portable radio equipment according to claim 10, wherein the internal conductive shield is made of conductive coating or conductive material.
 16. The portable radio equipment according to any preceding claim, wherein the electromagnetic shielding material includes an internal conductive body and an external conductive body.
 17. The portable radio equipment according to any preceding claim, wherein a nonconductive frame body is disposed on the electromagnetic shielding material.

Patentansprüche

1. Tragbare Funkvorrichtung, ausgestattet mit einer Antenne (103) zum Senden und Empfangen elektromagnetischer Wellen, einem Gehäuse (102), auf welchem die Antenne angebracht ist und welches einen Einschnitt (101) darin aufweist, wobei das Gehäuse aus einem elektromagnetisch abschirmenden Material besteht, und einer mit der Antenne (103) verbundenen Innenschaltung zum Erzeugen und Empfangen der elektromagnetischen Wellen.

- len über die Antenne (103),
 dadurch gekennzeichnet, daß
 der Einschnitt (101) in dem Gehäuse (102) in
 einer Weise angeordnet ist, daß das Strahlungsdiagramm modifiziert wird, welches von auf dem Gehäuse (102) fließenden Hochfrequenzströmen bewirkt wird.
2. Tragbare Funkvorrichtung nach Anspruch 1, wobei die Antenne (103) eine umgedrehte F-Typ-Miniaturantenne ist, welche auf dem Gehäuse (102) angeordnet ist.
 3. Tragbare Funkvorrichtung nach Anspruch 1, wobei die Antenne (103) eine Miniaturantenne (103) ist, welche über einer Oberseite des Gehäuses (102) angeordnet ist.
 4. Tragbare Funkvorrichtung nach einem der vorstehenden Ansprüche, wobei die Antenne (103) etwa die Länge eines Viertels der Wellenlänge aufweist und der Einschnitt (101) in einem Abstand von etwa einer Viertelwellenlänge von einem oberen Ende des Gehäuses (102) entfernt ist.
 5. Tragbare Funkvorrichtung nach einem der vorstehenden Ansprüche, wobei der Einschnitt (101) etwa eine Viertelwellenlänge lang ist.
 6. Tragbare Funkvorrichtung nach einem der vorstehenden Ansprüche, wobei mehrere Einschnitte (101) in dem Gehäuse (102) angeordnet sind.
 7. Tragbare Funkvorrichtung nach einem der vorstehenden Ansprüche, wobei die Innenschaltung eine erste Schaltung (202) zum Senden der elektromagnetischen Welle und eine zweite Schaltung (201) zum Empfangen der elektromagnetischen Welle enthält, und die erste Schaltung in einem Abschnitt über dem Einschnitt in einem Fall angeordnet, bei welchem die zweite Schaltung in einem Abschnitt unter dem Einschnitt angeordnet ist.
 8. Tragbare Funkvorrichtung nach einem der vorstehenden Ansprüche, wobei ein ferromagnetisches Material (111) um einen Teil des Umfanges des Gehäuses (102) herum angebracht ist.
 9. Tragbare Funkvorrichtung nach einem der vorstehenden Ansprüche, wobei das Gehäuse (102) eine mit der Antenne (103) verbundene Empfangseinrichtung (104) zum Empfangen einer elektromagnetischen Welle (S1) von der Antenne (103) und Ausgeben eines Signals (S2), wenn die Antenne (103) keine andere elektromagnetische Welle (103) empfängt und die elektromagnetische Welle nicht sendet, eine mit der Antenne (103) und der Empfangseinrichtung (104) verbundene Bewertungs-
 - einrichtung (120) zum Detektieren einer Fehlerrate der einen von der Antenne (103) gelieferten elektromagnetischen Welle (S1) und zum Ausgeben eines Bewertungssignals (S3) auf der Basis der einen detektierten elektromagnetischen Welle, wenn das Signal (S2) aus der Empfangseinrichtung (104) empfangen wird, eine mit der Bewertungseinrichtung (120) verbundene Schaltertreibereinrichtung (121) zum Empfangen des Bewertungssignals (S3) aus der Bewertungsschaltung (120) und zum Ausgeben eines Steuersignals (S4) auf der Basis des empfangenen Bewertungssignals (S3), und eine Schalteinrichtung (122) enthält, die in der Nähe eines offenen Endes der Einschnittes (101) angeordnet und mit der Schaltertreibereinrichtung (121) verbunden ist, um das offene Ende (101) als Antwort auf das von der Schaltertreibereinrichtung (121) gelieferte Steuersignal (S4) elektrisch zu öffnen oder kurzzuschließen (Fig. 38).
 10. Tragbare Funkvorrichtung nach einem der vorstehenden Ansprüche, wobei das Gehäuse (102) eine darin befindliche leitende Innenabschirmung aufweist (Fig. 37).
 11. Tragbare Funkvorrichtung nach Anspruch 10, wobei die leitende Innenabschirmung ein Innengehäuseteil (102-b) und ein Außengehäuseteil (102-a) mit einem Einschnitt darin enthält, das Innengehäuseteil (102-b) und das Außengehäuseteil (102-a) aus einem elektrisch leitenden Material bestehen und eine leitende Beschichtung und Plattierung wie z.B. eine Aluminiumplattierung und Nickelplattierung, Kupfer, Aluminium oder ein daraus kombiniertes Material enthalten, und das Innengehäuseteil (102-b) und das Außengehäuseteil (102-a) gegeneinander isoliert sind (Fig. 37, 39, 40).
 12. Tragbare Funkvorrichtung nach Anspruch 10, wobei das Gehäuse (102) ferner ein nichtleitendes Rahmengehäuseteil aufweist, welches auf der leitenden Innenabschirmung angeordnet ist.
 13. Tragbare Funkvorrichtung nach einem der vorstehenden Ansprüche, wobei mehrere Monopolantennen, welche eine Länge einer Viertelwellenlänge aufweisen, auf dem Gehäuse (102) angebracht sind.
 14. Tragbare Funkvorrichtung nach Anspruch 13, wobei mehrere umgedrehte F-Antennen oder Wendelantennen, oder diese in Kombination auf dem Gehäuse (102) angeordnet sind, um so eine Diversity-Anordnung zu bilden.
 15. Tragbare Funkvorrichtung nach Anspruch 10, wobei die leitende Innenabschirmung aus einer leitenden Beschichtung oder einem leitenden Material

besteht.

16. Tragbare Funkvorrichtung nach einem der vorstehenden Ansprüche, wobei das elektromagnetische Abschirmungsmaterial ein leitenden Innengehäuseteil und ein leitendes Außengehäuseteil umfaßt.

17. Tragbare Funkvorrichtung nach einem der vorstehenden Ansprüche, wobei ein nichtleitendes Rahmengehäuseteil auf dem elektromagnetischen Abschirmungsmaterial angeordnet ist.

Revendications

1. Equipement de radio portable comportant une antenne (103) pour transmettre et recevoir des ondes électromagnétiques, un logement (102) sur lequel l'antenne est montée et comprenant une encoche (101), ledit logement étant constitué d'un matériau de protection électromagnétique, et un circuit interne connecté à l'antenne (103) pour produire et recevoir les ondes électromagnétiques par l'intermédiaire de l'antenne (103),

caractérisé en ce que :

- l'encoche (101) est disposée dans le logement (102) de manière à modifier le diagramme de rayonnement provoqué par les courants de haute fréquence circulant sur le logement (102).

2. Equipement de radio portable selon la revendication 1, dans lequel l'antenne (103) est une antenne miniature du type en F inversé (103) disposée sur le logement (102).

3. Equipement de radio portable selon la revendication 1, dans lequel l'antenne (103) est une antenne du type miniature (103) disposée sur la partie supérieure du logement (102).

4. Equipement de radio portable selon l'une quelconque des revendications précédentes, dans lequel l'antenne (103) a approximativement une longueur d'un quart de longueur d'onde et l'encoche (101) est disposée à une distance d'environ un quart de longueur d'onde par rapport à l'extrémité supérieure du logement (102).

5. Equipement de radio portable selon l'une quelconque des revendications précédentes, dans lequel l'encoche (101) a une longueur d'environ un quart de longueur d'onde.

6. Equipement de radio portable selon l'une quelconque des revendications précédentes, dans lequel une multitude d'encoches (101) sont disposées

dans le logement (102).

7. Equipement de radio portable selon l'une quelconque des revendications précédentes, dans lequel le circuit interne comporte un premier circuit (202) pour transmettre l'onde électromagnétique et un second circuit (201) pour recevoir l'onde électromagnétique, et le premier circuit est disposé dans la partie supérieure de l'encoche dans le cas où le second circuit est placé dans la partie inférieure de l'encoche (figures 33-34).

8. Equipement de radio portable selon l'une quelconque des revendications précédentes, dans lequel un matériau ferromagnétique (111) est fixé autour d'une partie de la circonférence du logement (102).

9. Equipement de radio portable selon l'une quelconque des revendications précédentes, dans lequel le logement (102) comporte un moyen de réception (104) connecté à l'antenne (103) pour recevoir une onde électromagnétique (S1) provenant de l'antenne (103) et sortir un signal (S2) lorsque l'antenne (103) ne reçoit pas une autre onde électromagnétique et ne transmet pas l'onde électromagnétique, un moyen d'évaluation (120) connecté à l'antenne (103) et au moyen de réception (104) pour détecter un taux d'erreur de cette onde électromagnétique (S1) fournie à partir de l'antenne (103) et sortir un signal d'évaluation (S3) sur la base de l'onde électromagnétique détectée lors de la réception du signal (S2) provenant du moyen de réception (104), un moyen d'attaque de commutateur (121) connecté au moyen d'évaluation (120) pour recevoir le signal d'évaluation (S3) en provenance du moyen d'évaluation (120) et sortir un signal de commande (S4) sur la base du signal d'évaluation reçu (S3), et un moyen de commutateur (122) disposé dans le voisinage de l'extrémité ouverte de l'encoche (101) et connecté au moyen d'attaque de commutateur (121) pour ouvrir et court-circuiter électriquement l'extrémité ouverte de l'encoche (101) en réponse au signal de commande (S4) fourni à partir du moyen d'attaque de commutateur (121) (figure 38).

10. Equipement de radio portable selon l'une quelconque des revendications précédentes, dans lequel le logement (102) comporte intérieurement un écran conducteur interne (figure 37).

11. Equipement de radio portable selon la revendication 10, dans lequel l'écran conducteur interne comporte un corps interne (102-b) et un corps externe (102-a) comportant l'encoche, le corps interne (102-b) et le corps externe (102-a) sont constitués d'un matériau conducteur de l'électricité et comprennent un revêtement et un placage conducteurs tels qu'un placage d'aluminium et un placage de

nickel, du cuivre, de l'aluminium, ou un matériau obtenu par combinaison de ceux-ci, et le corps interne (102-b) et le corps externe (102-a) sont isolés l'un de l'autre (figures 37, 39, 41).

5

12. Equipement de radio portable selon la revendication 10, dans lequel le logement (102) comporte en outre un corps de châssis non conducteur disposé sur l'écran conducteur interne.

10

13. Equipement de radio portable selon l'une quelconque des revendications précédentes, dans lequel une multitude d'antennes monopolaires d'une longueur d'un quart de longueur d'onde sont montées sur le logement (102).

15

14. Equipement de radio portable selon la revendication 13, dans lequel une multitude d'antennes en F Inversé ou d'antennes hélicoïdales, ou en combinaison, sont disposées sur le logement (102) de manière à constituer une branche de diversité.

20

15. Equipement de radio portable selon la revendication 10, dans lequel l'écran conducteur interne est constitué d'un revêtement conducteur ou d'un matériau conducteur.

25

16. Equipement de radio portable selon l'une quelconque des revendications précédentes, dans lequel le matériau de protection électromagnétique comprend un corps conducteur interne et un corps conducteur externe.

30

17. Equipement de radio portable selon l'une quelconque des revendications précédentes, dans lequel un corps de châssis non conducteur est disposé sur le matériau de protection électromagnétique.

35

40

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50

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FIG.1
PRIOR ART

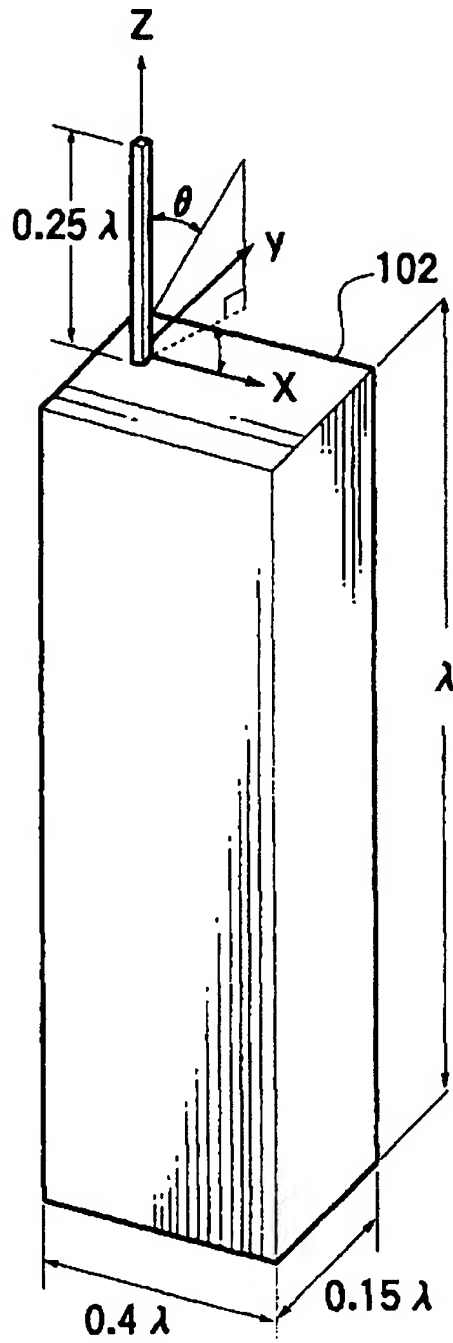


FIG.2A
PRIOR ART

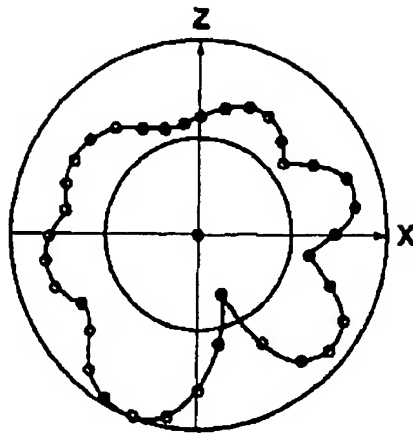


FIG.2B
PRIOR ART

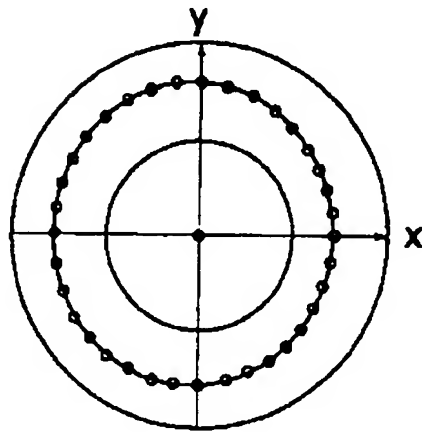


FIG.2C
PRIOR ART

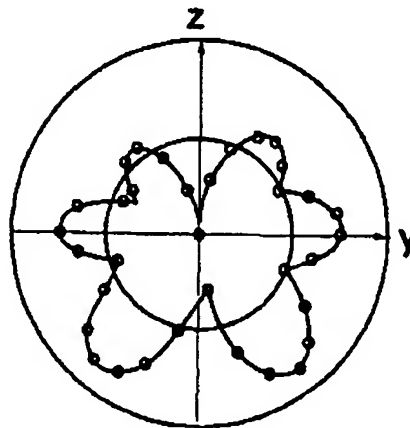


FIG.3A

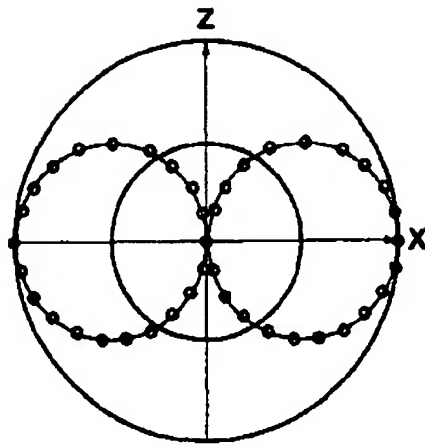


FIG.3B

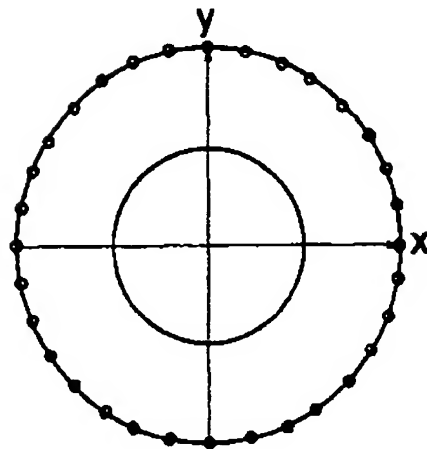


FIG.3C

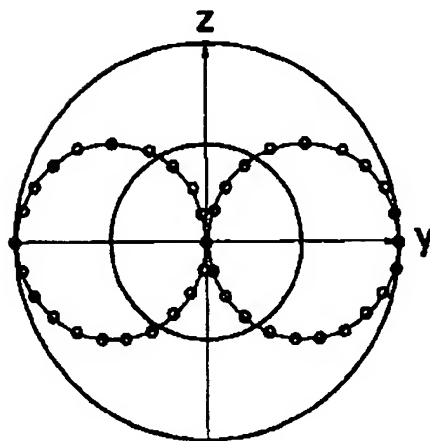


FIG. 4
PRIOR ART

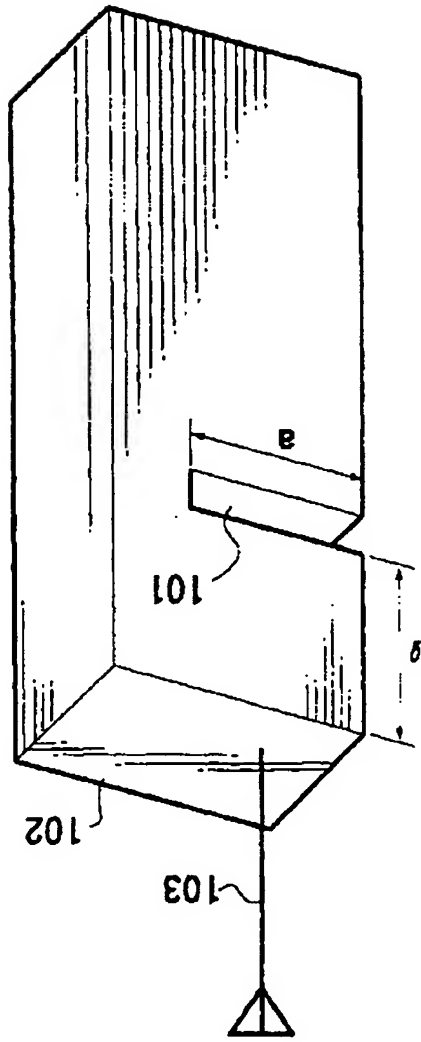
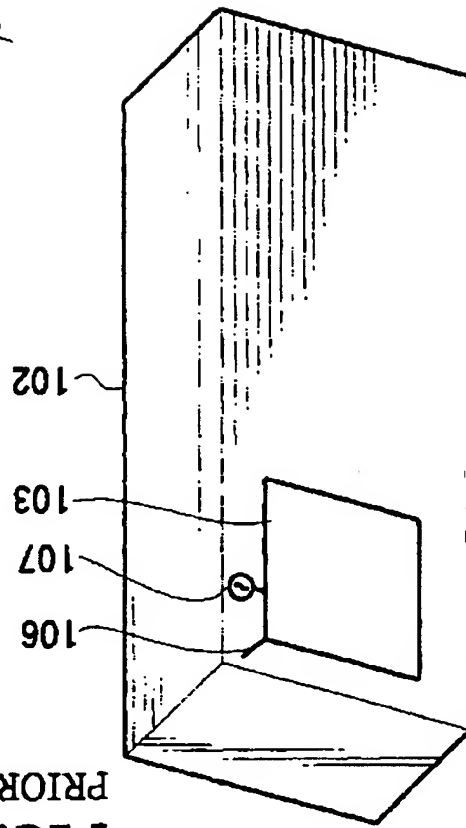


FIG. 6

FIG.5A
PRIOR ART

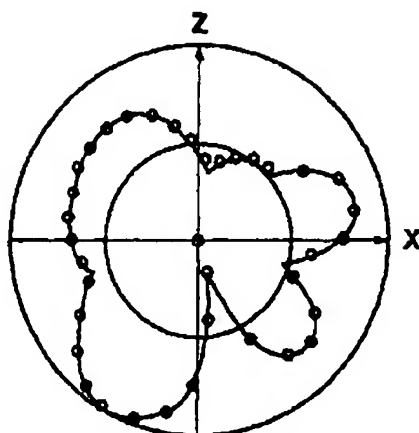


FIG.5B
PRIOR ART

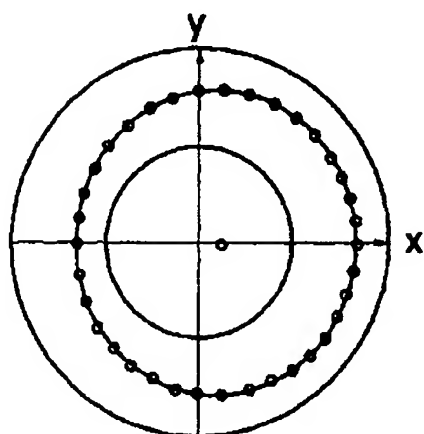


FIG.5C
PRIOR ART

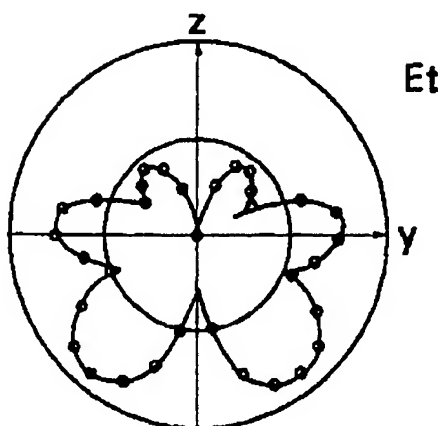


FIG.7

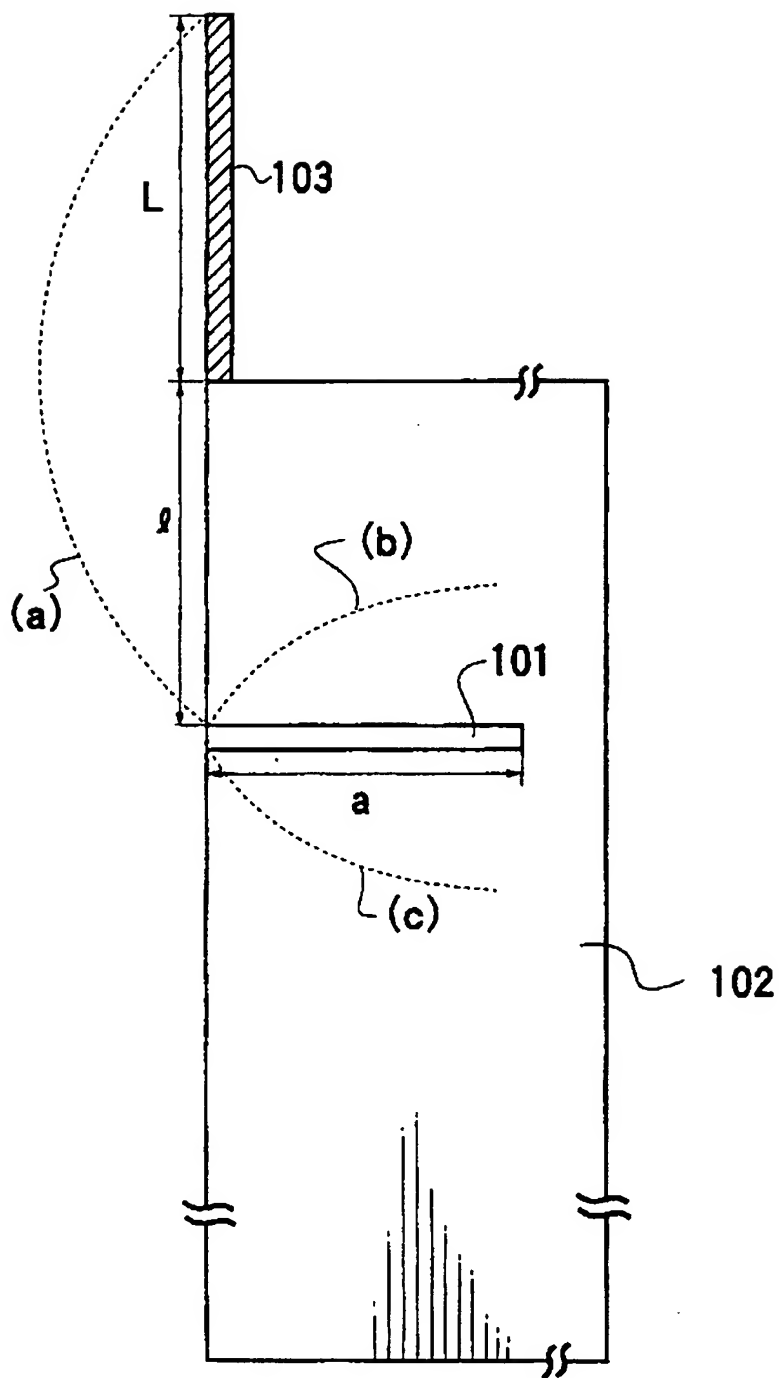


FIG.8

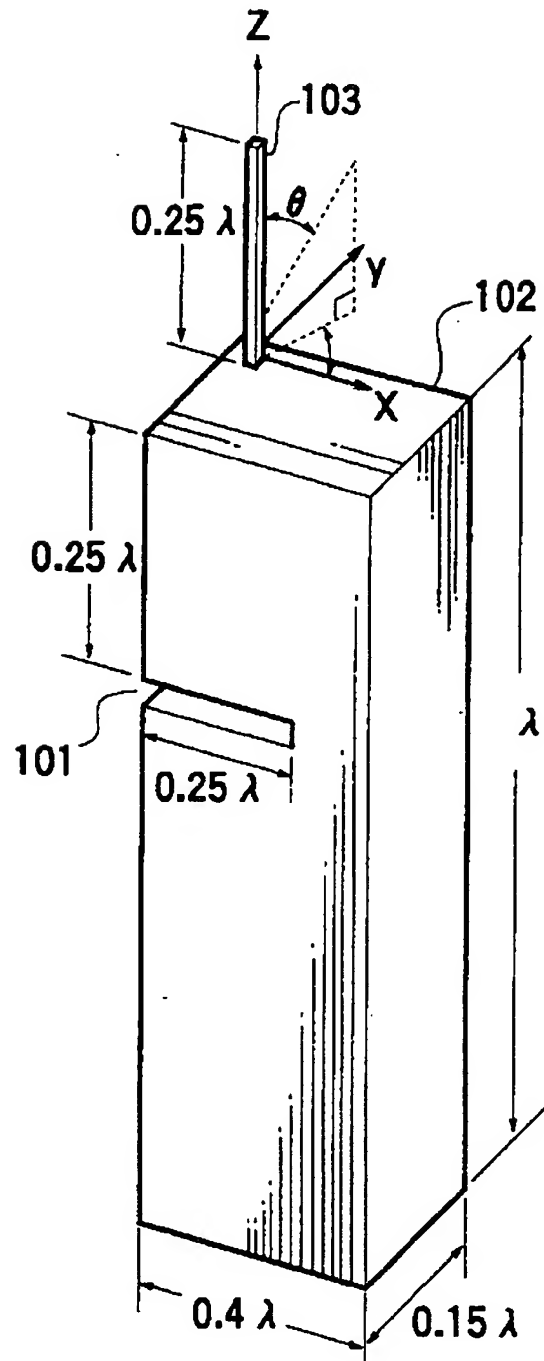


FIG.9A

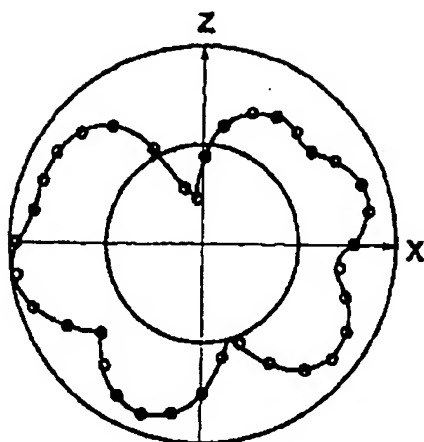


FIG.9B

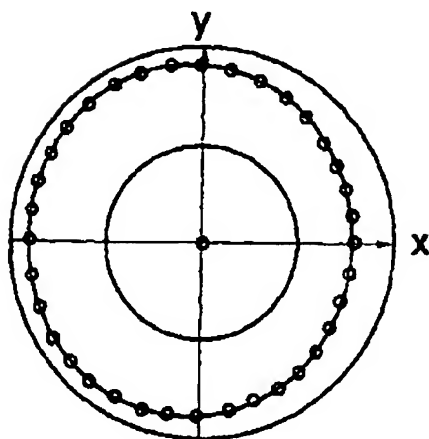
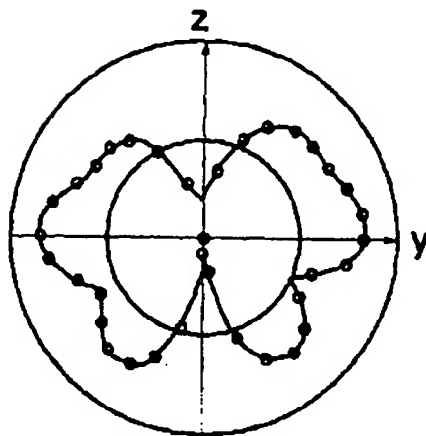


FIG.9C



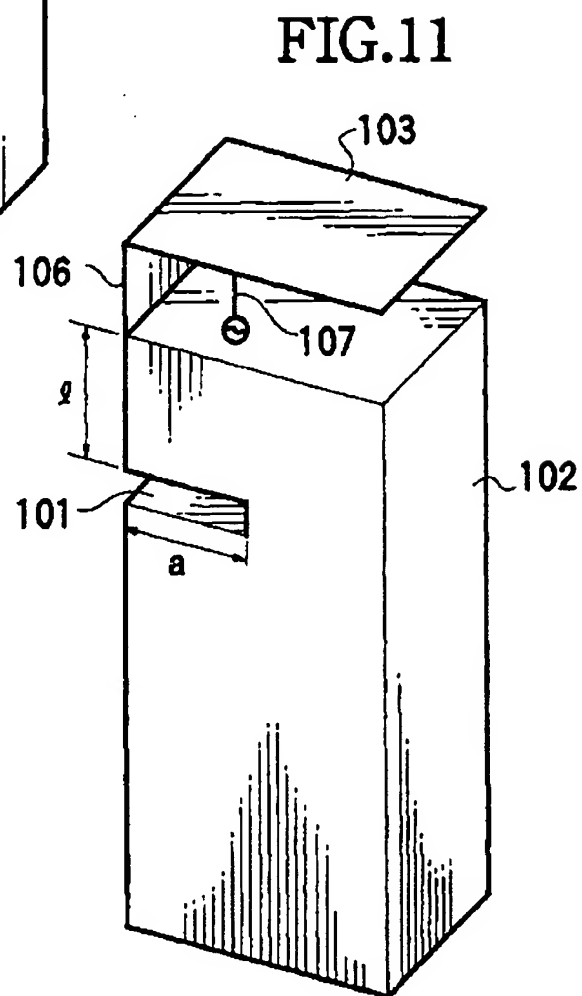
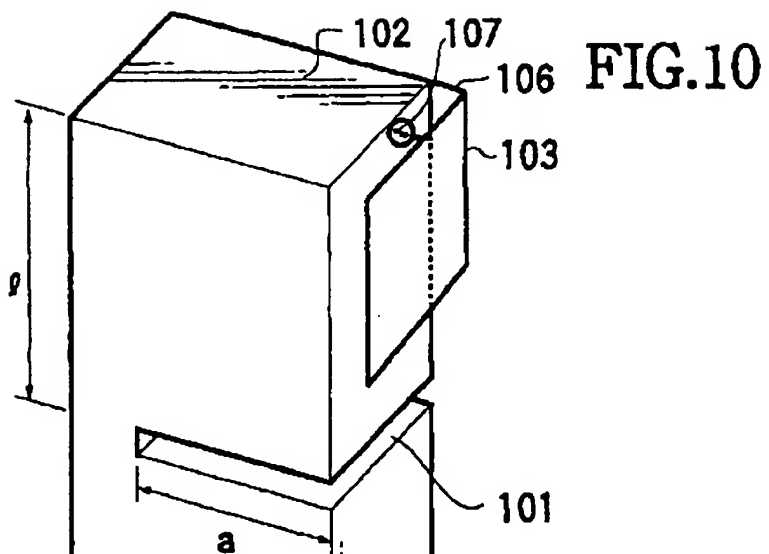


FIG.12

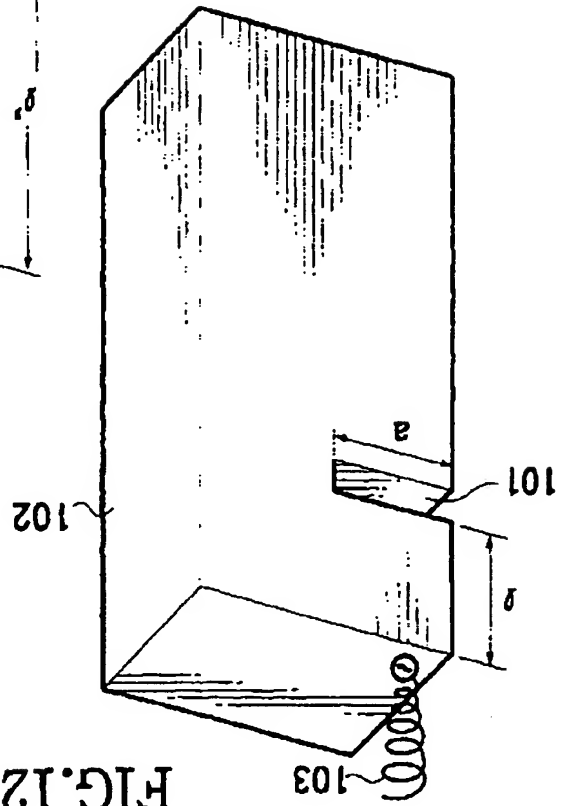


FIG.13

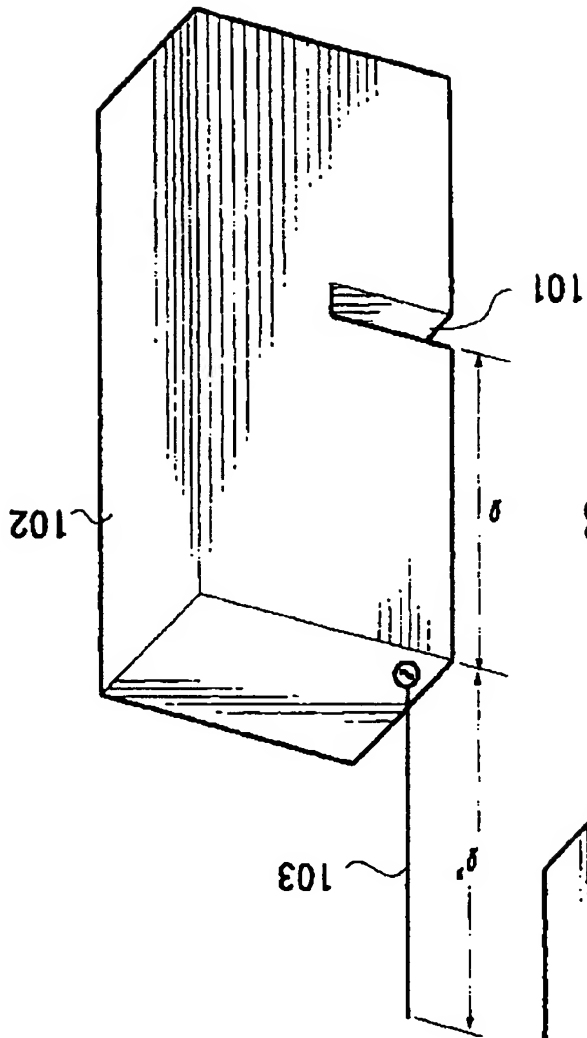


FIG.14

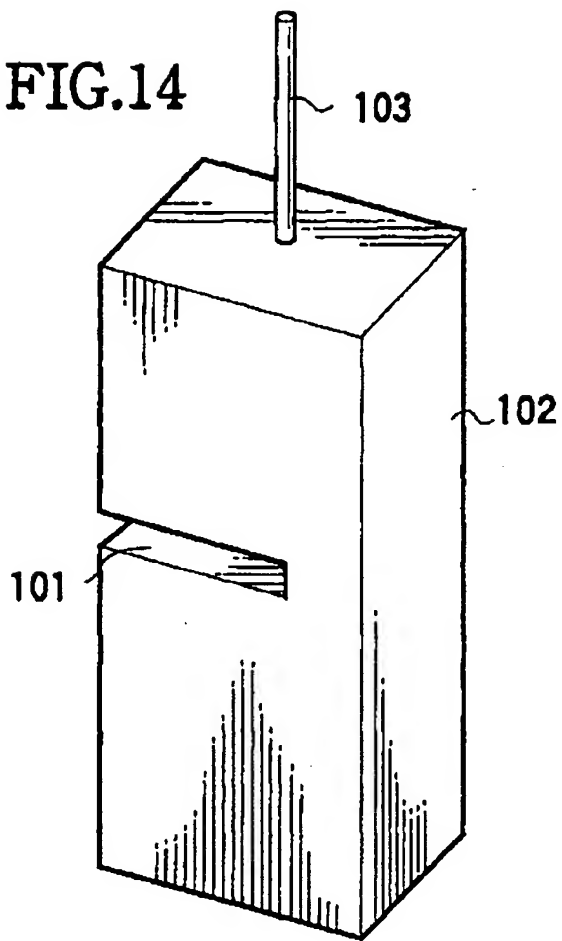


FIG.15A

$$a = 3/16 \lambda$$

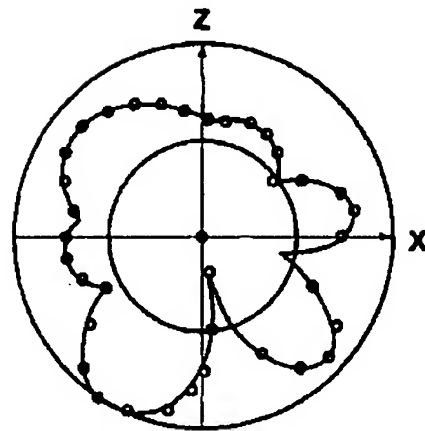


FIG.15B

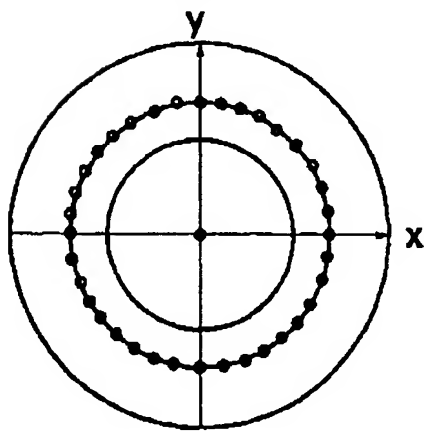


FIG.15C

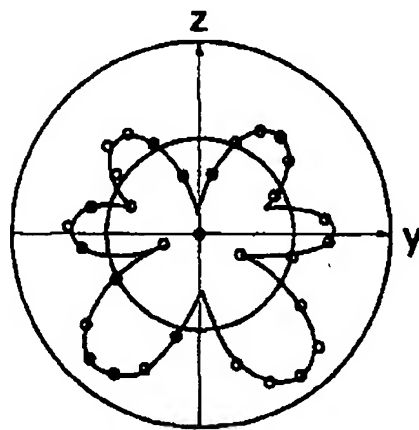


FIG.16A

$$a = 1/5 \lambda$$

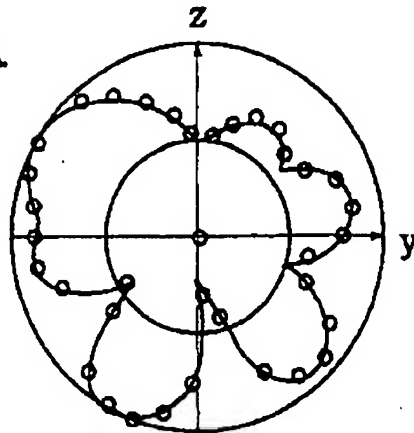


FIG.16B

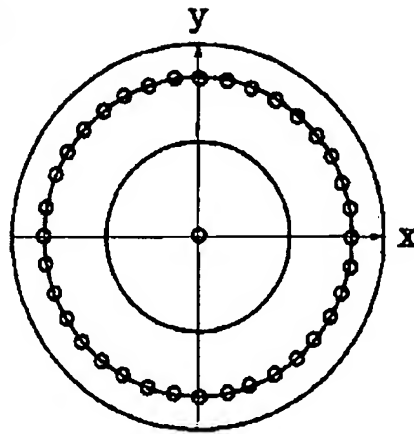


FIG.16C

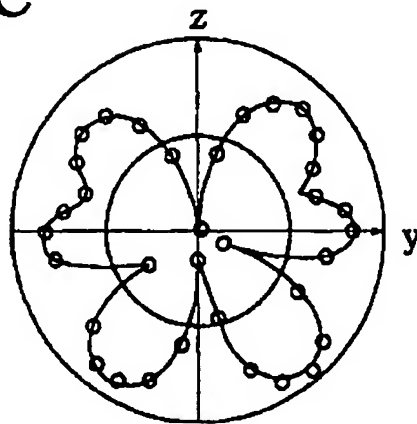


FIG.17A

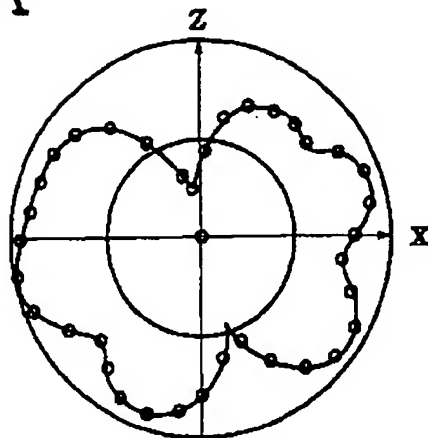


FIG.17B

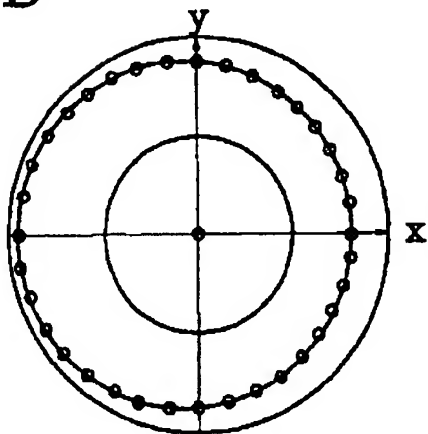


FIG.17C

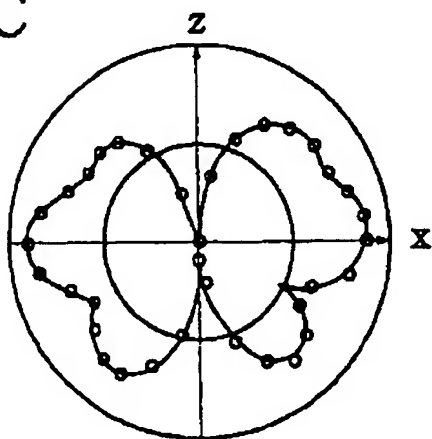
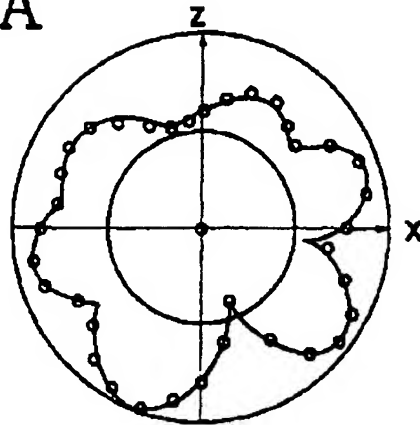


FIG.18A



$$a = \lambda / 3$$

FIG.18B

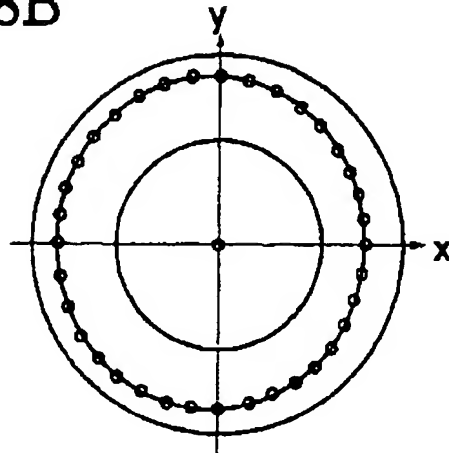


FIG.18C

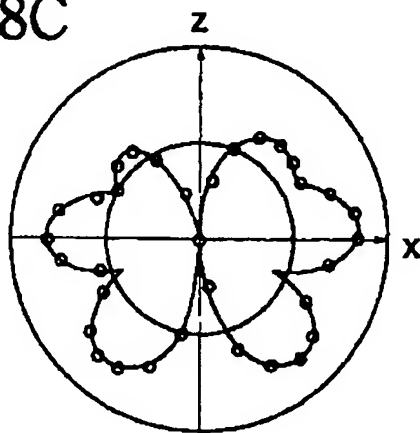


FIG.19

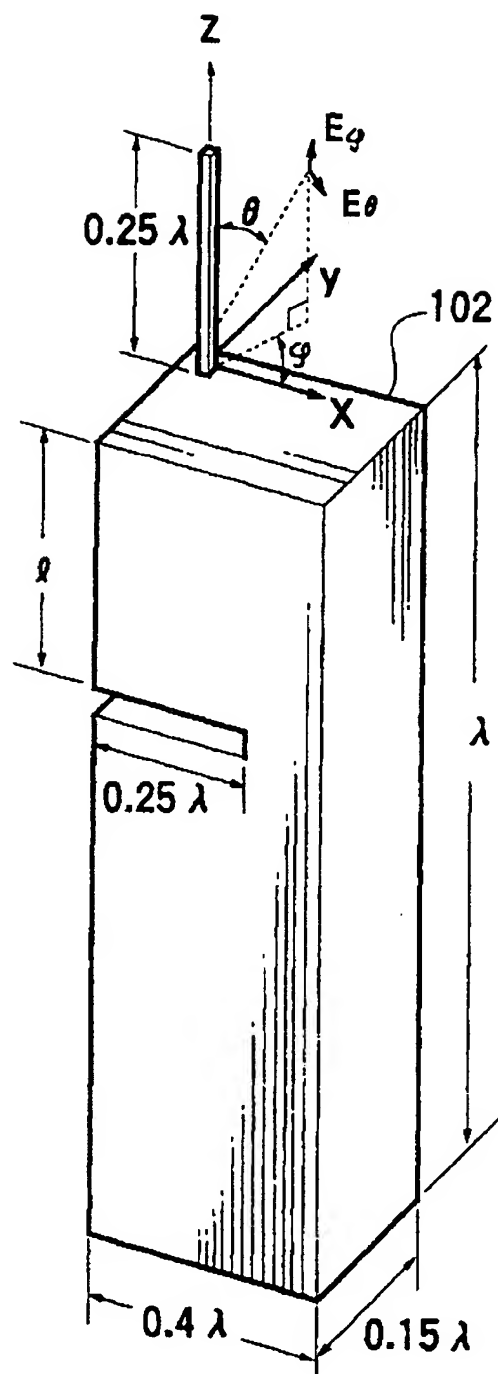


FIG.20A

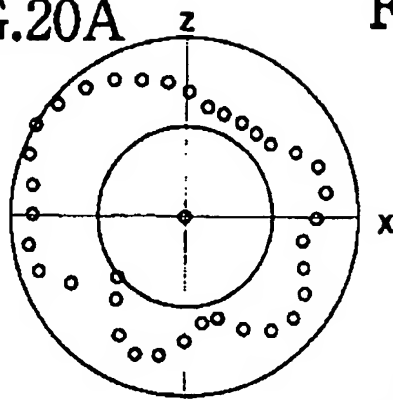


FIG.20B

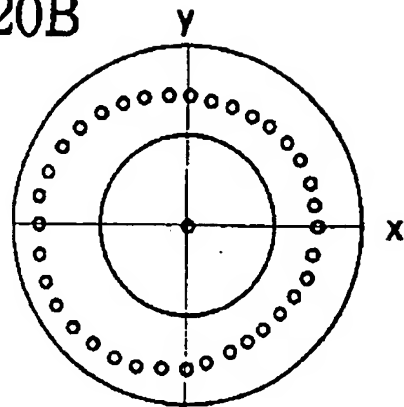
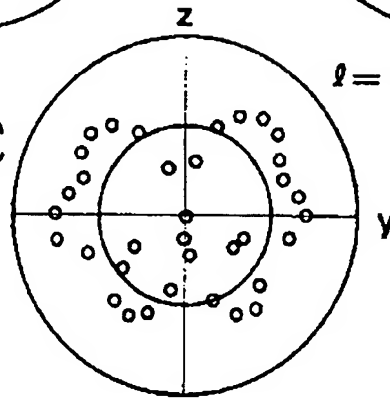


FIG.20C



$$l = \lambda / 16 \ (0.0625 \lambda)$$

FIG.21A

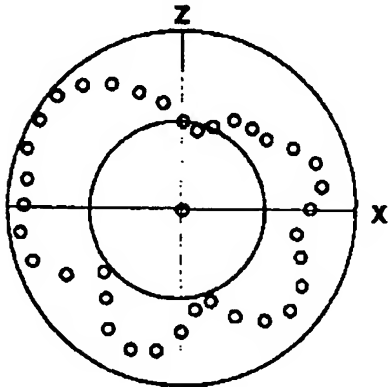


FIG.21B

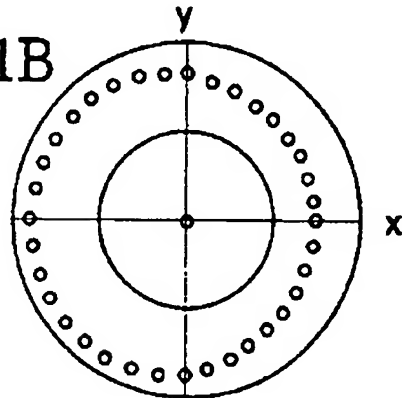
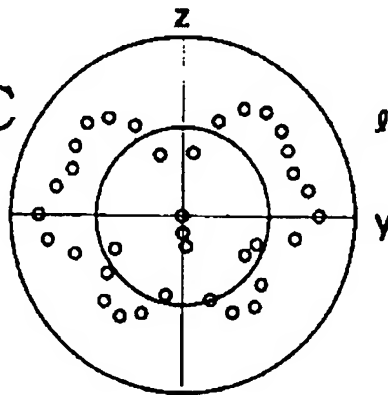


FIG.21C



$$l = 5/48 \lambda \ (0.104 \lambda)$$

FIG.22A

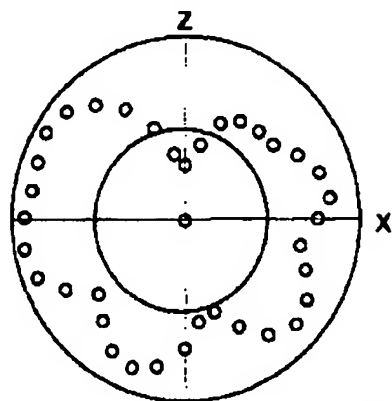


FIG.22B

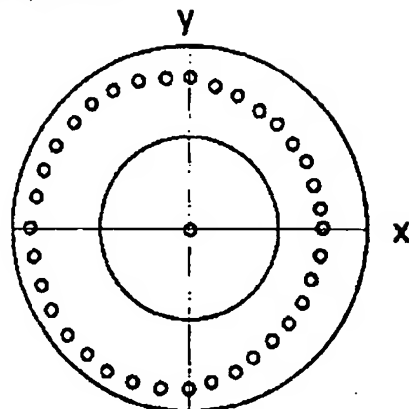
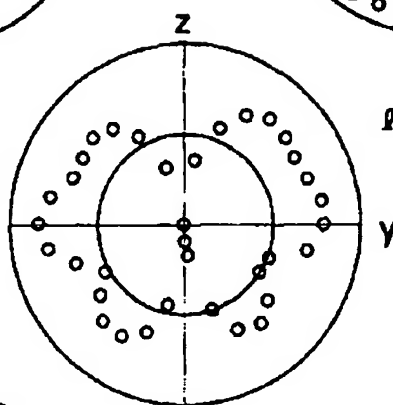


FIG.22C



$$l = 3/16 \lambda (0.188 \lambda)$$

FIG.23A

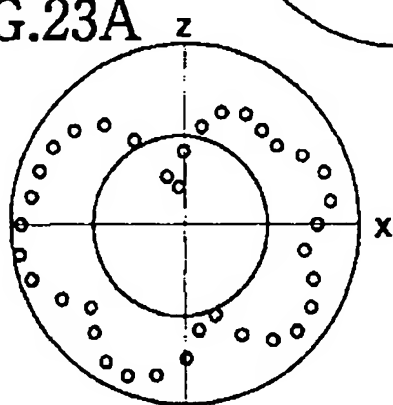


FIG.23B

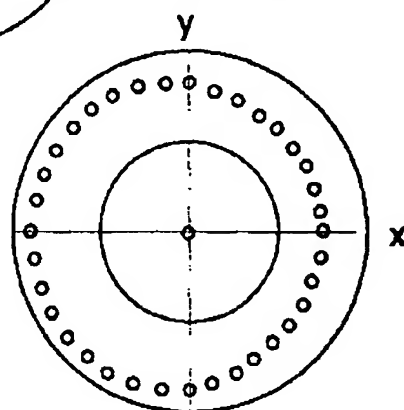
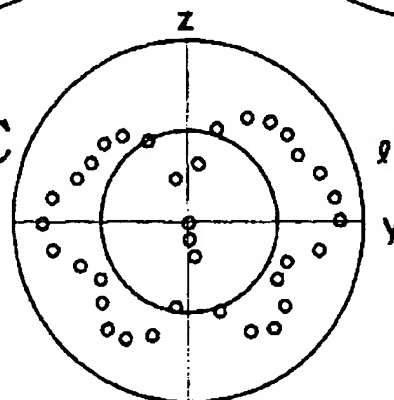
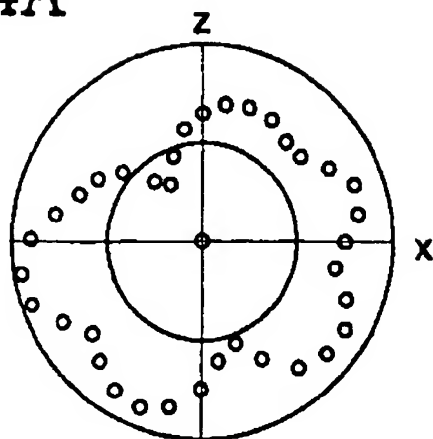


FIG.23C



$$l = \lambda / 4 (0.25 \lambda)$$

FIG.24A



$$l = 5/16 \lambda \quad (0.313 \lambda)$$

FIG.24B

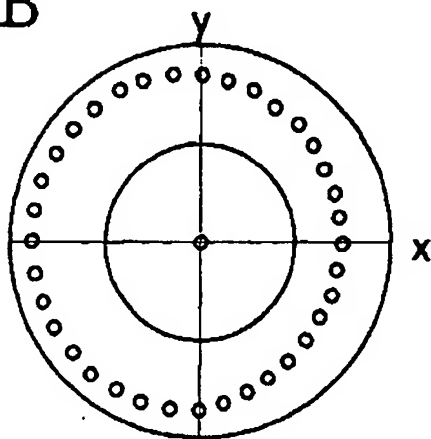


FIG.24C

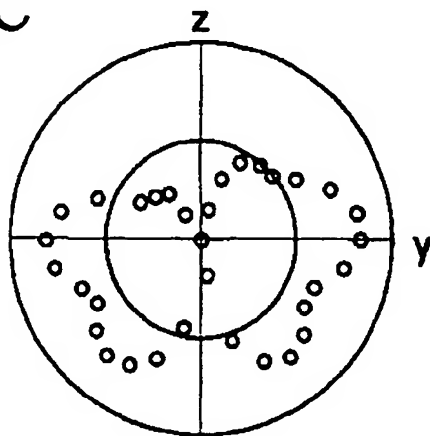


FIG.25

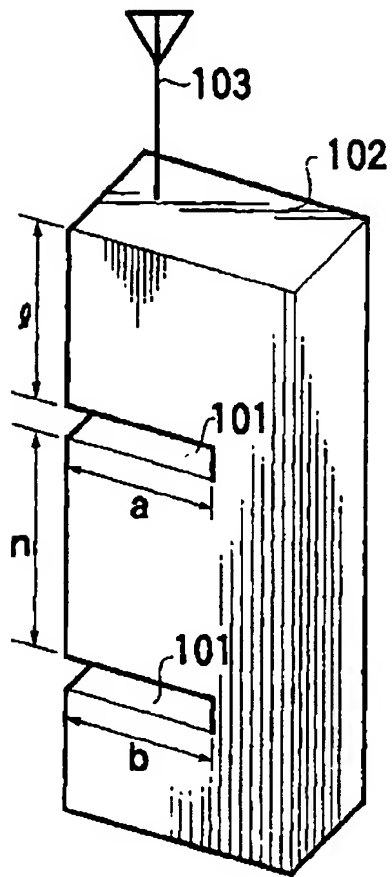


FIG.26

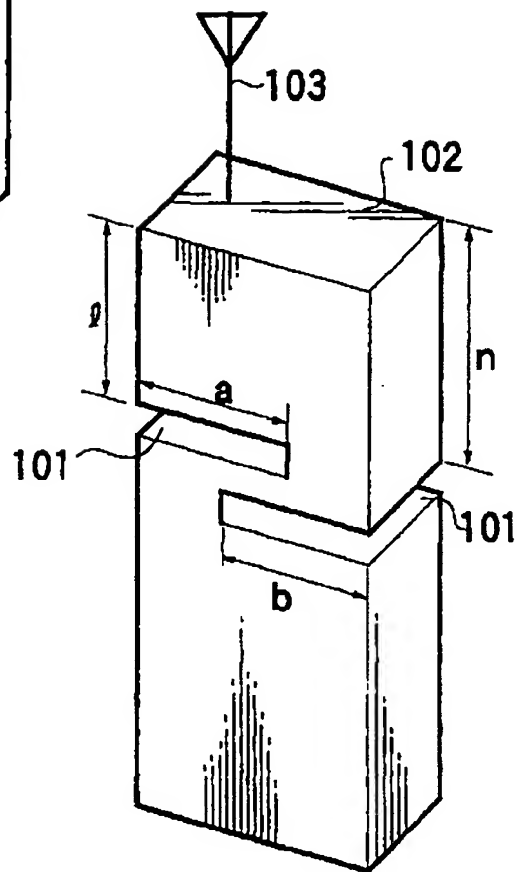


FIG. 27

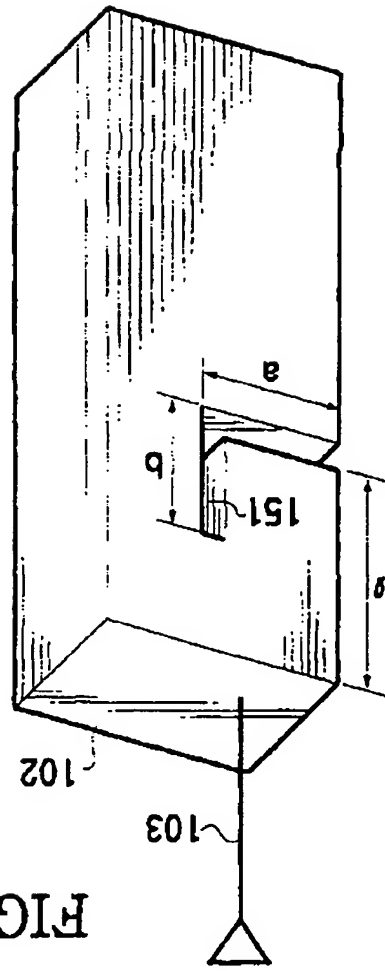


FIG. 28

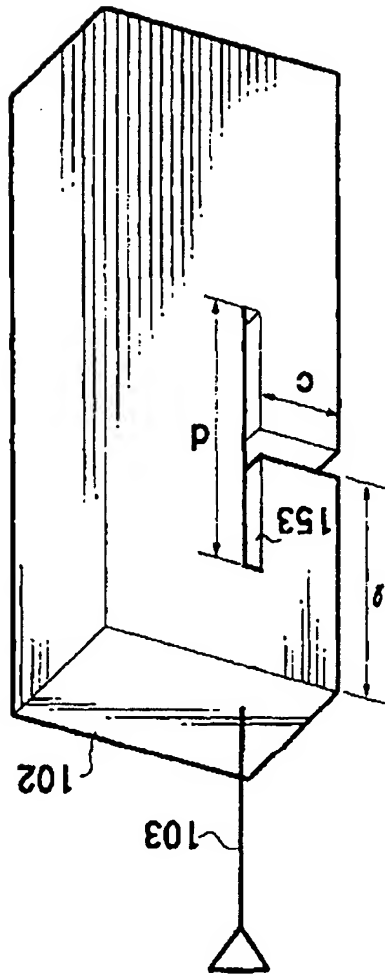


FIG.29A

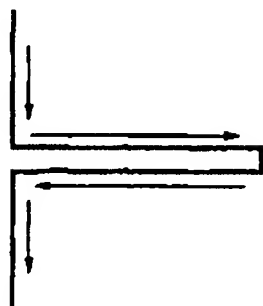


FIG.29B

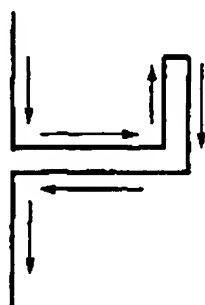


FIG.29C



FIG.30

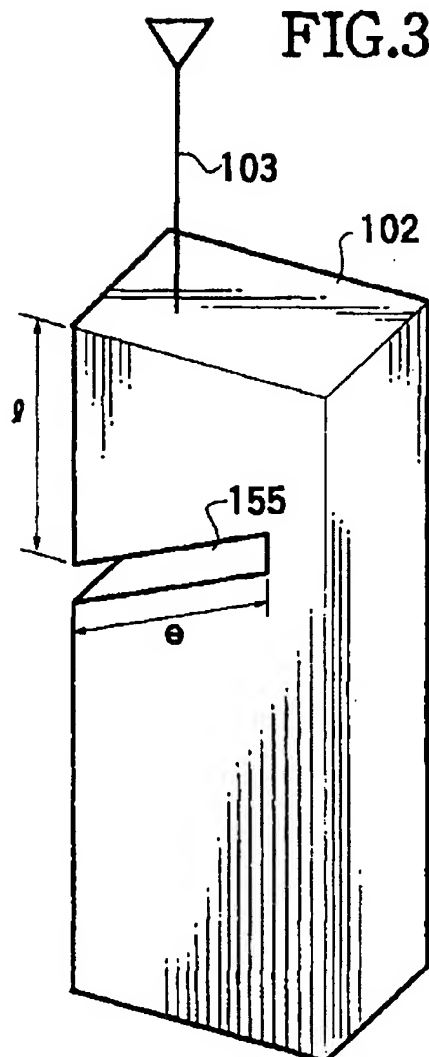
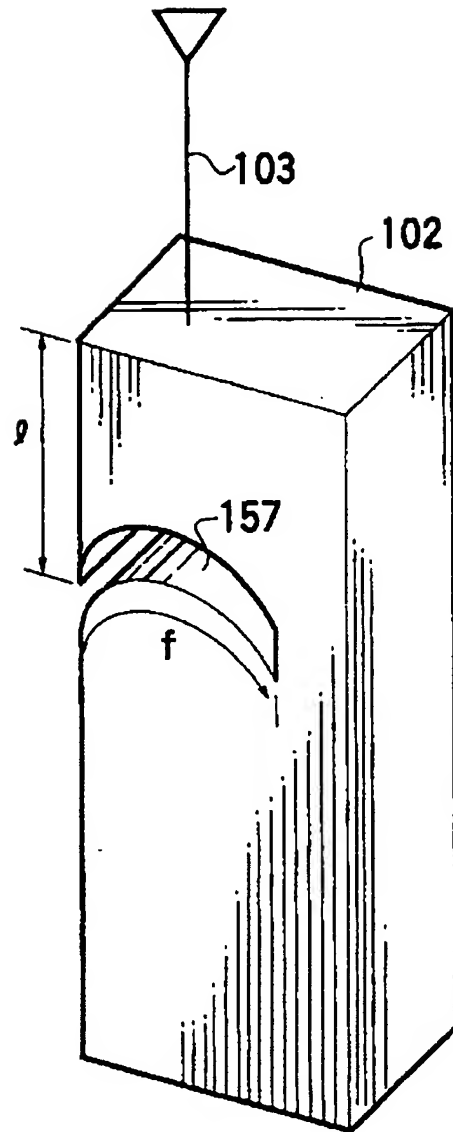


FIG.31



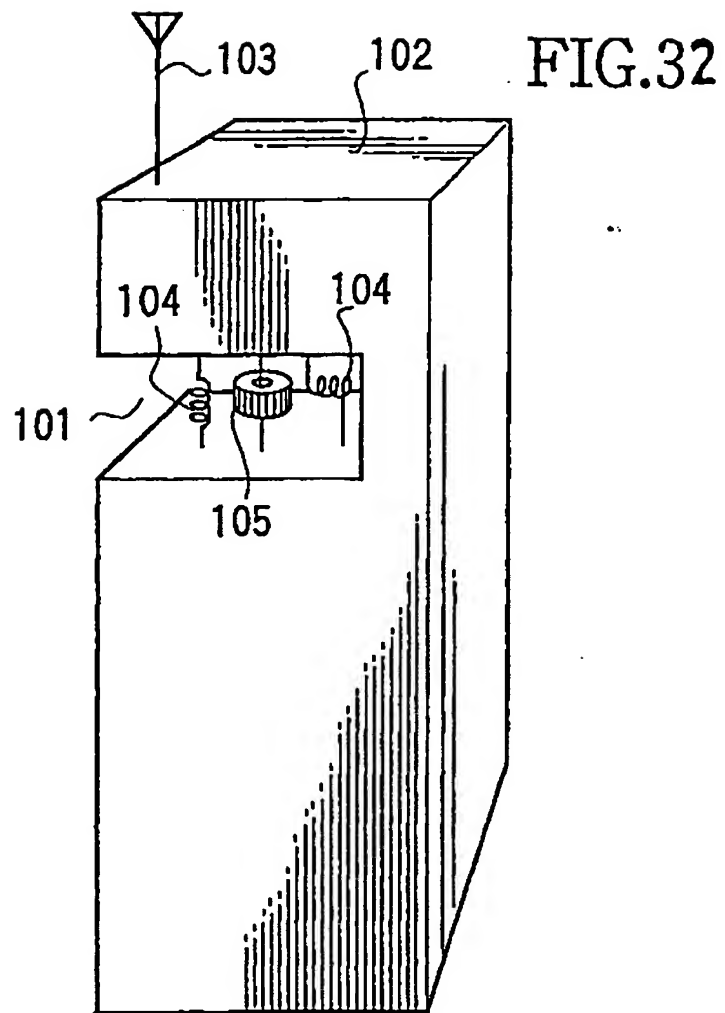


FIG.33

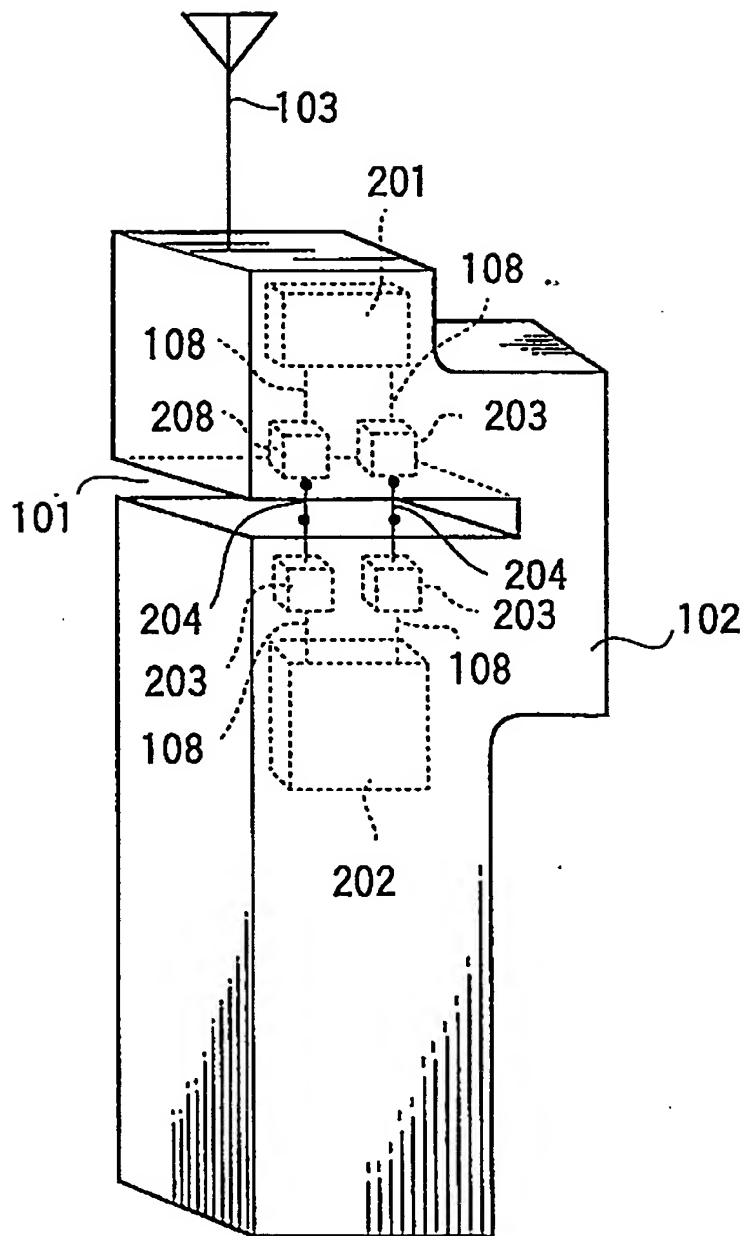
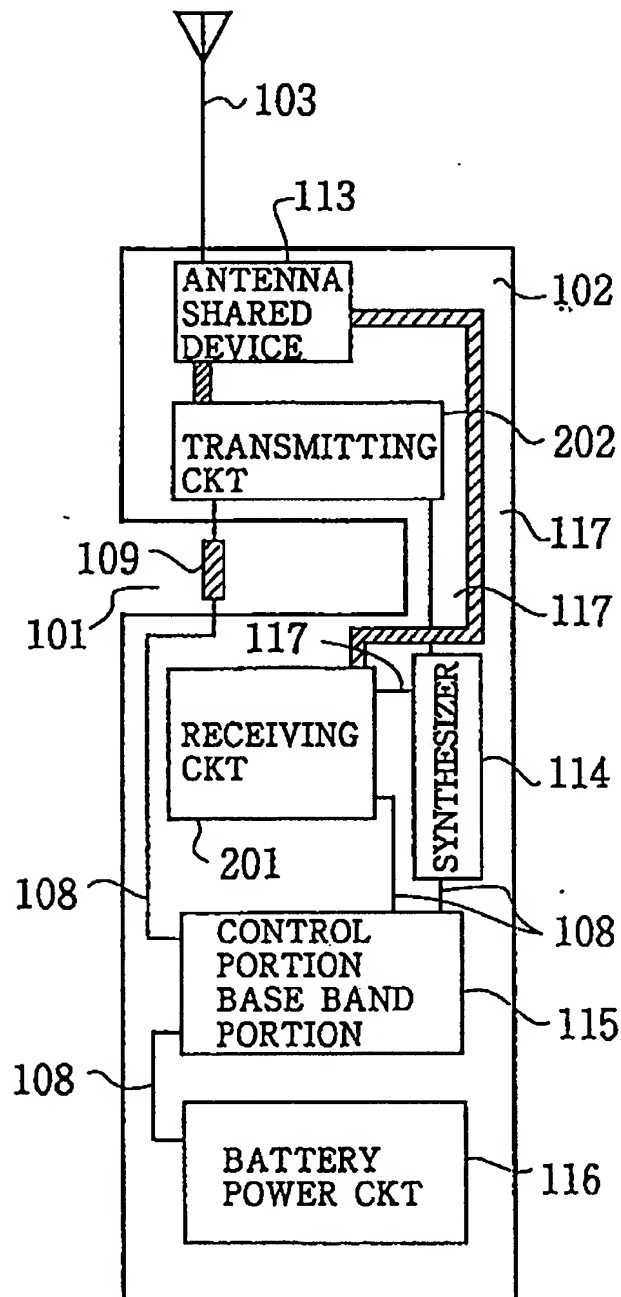
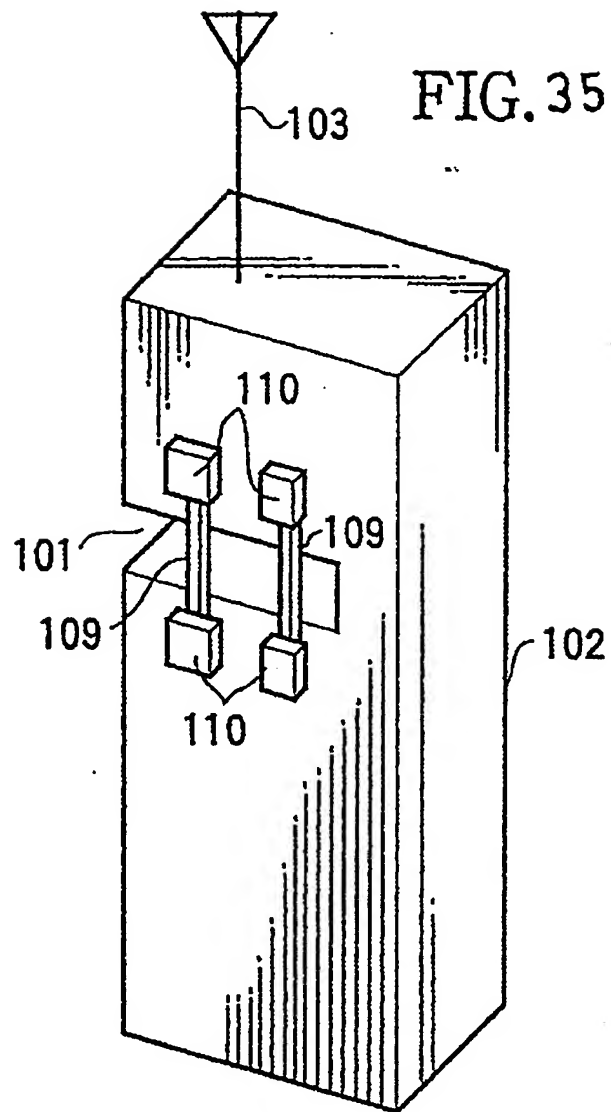


FIG.34





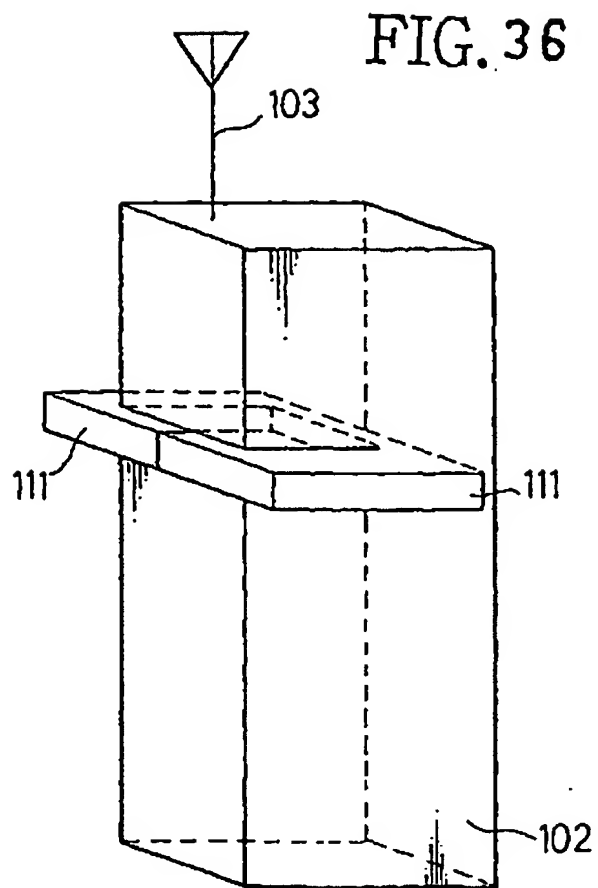


FIG. 37

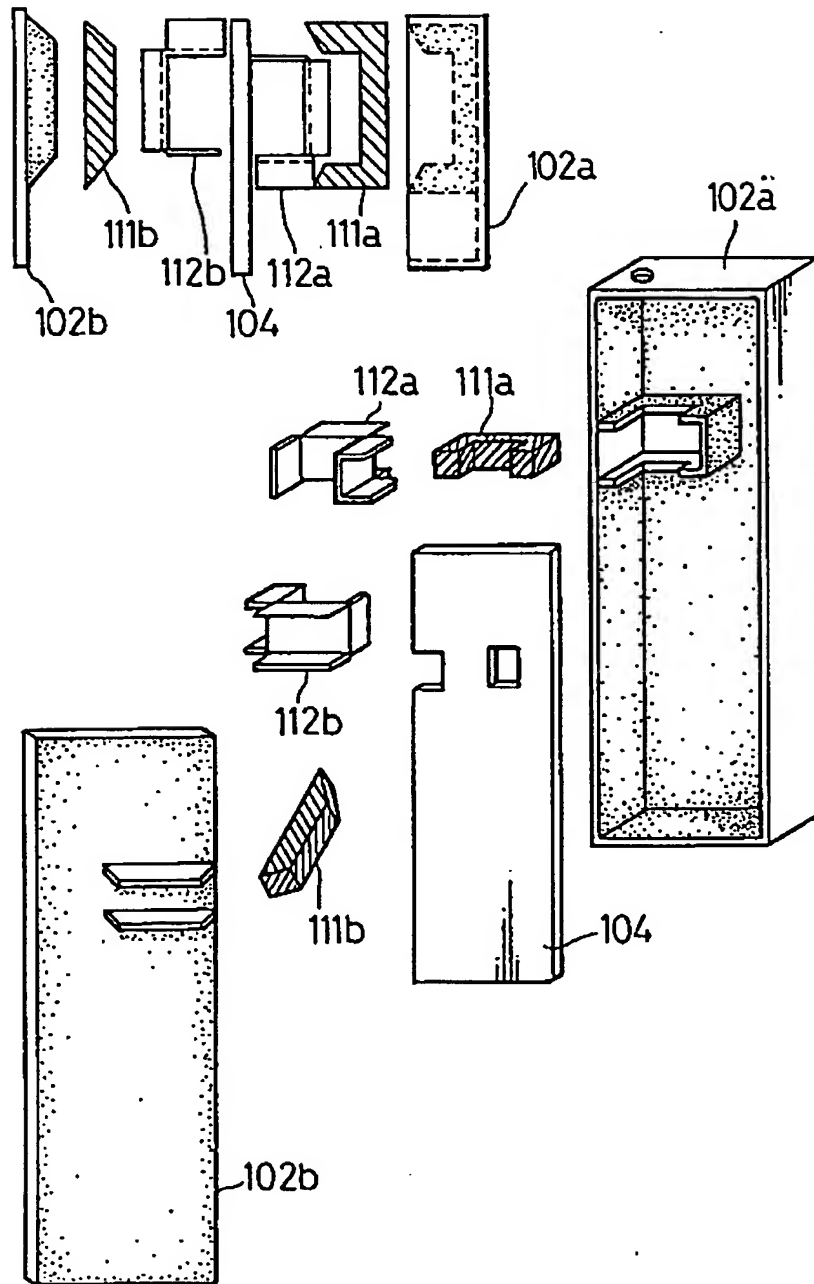
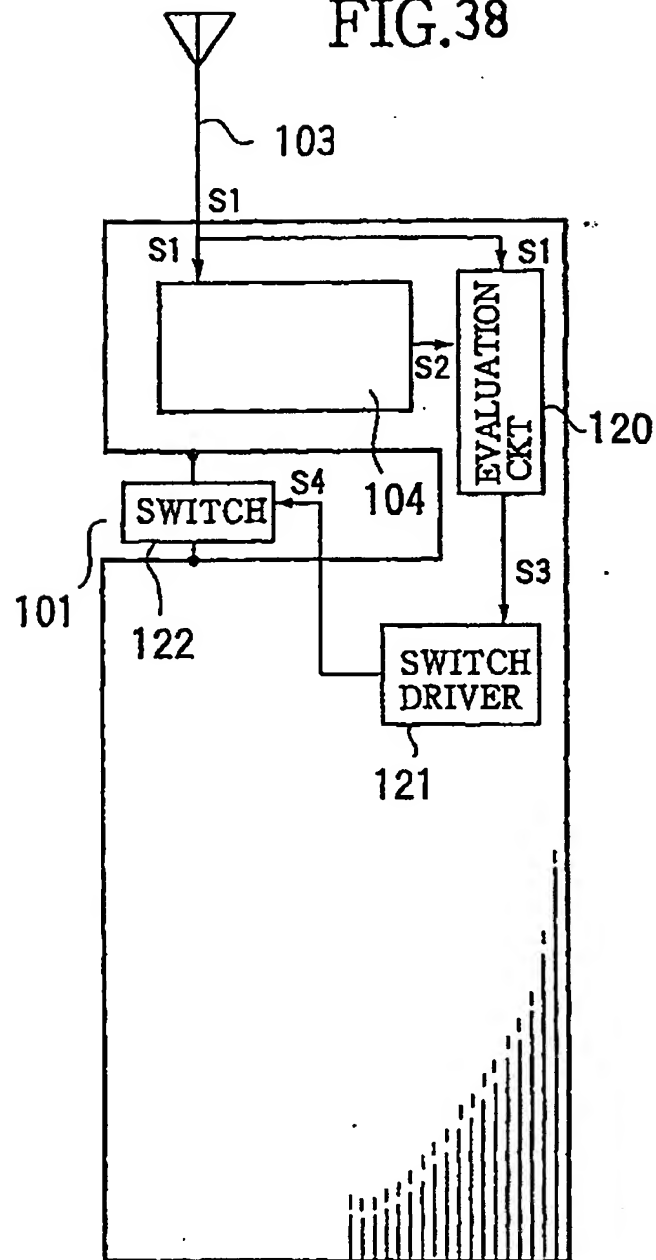


FIG.38



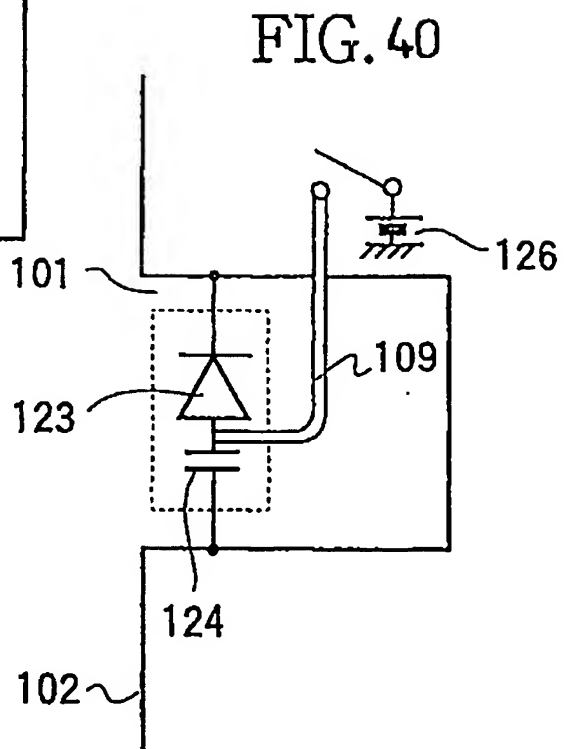
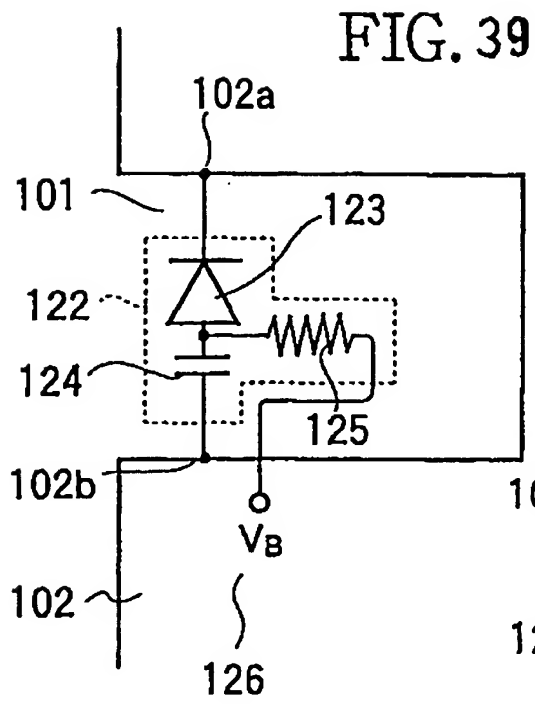


FIG. 41

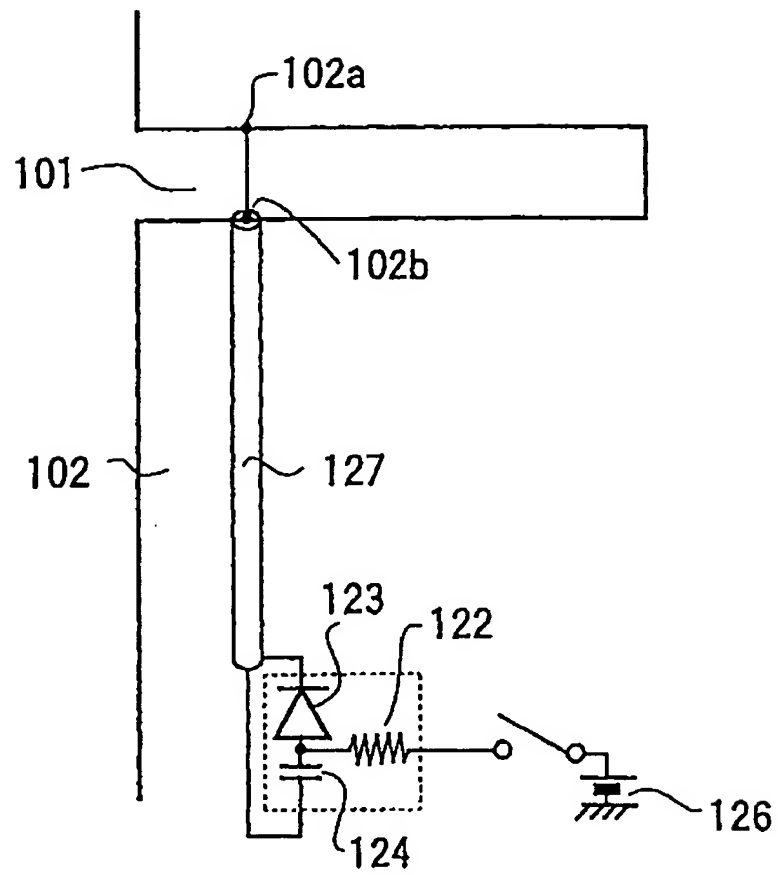


FIG. 42

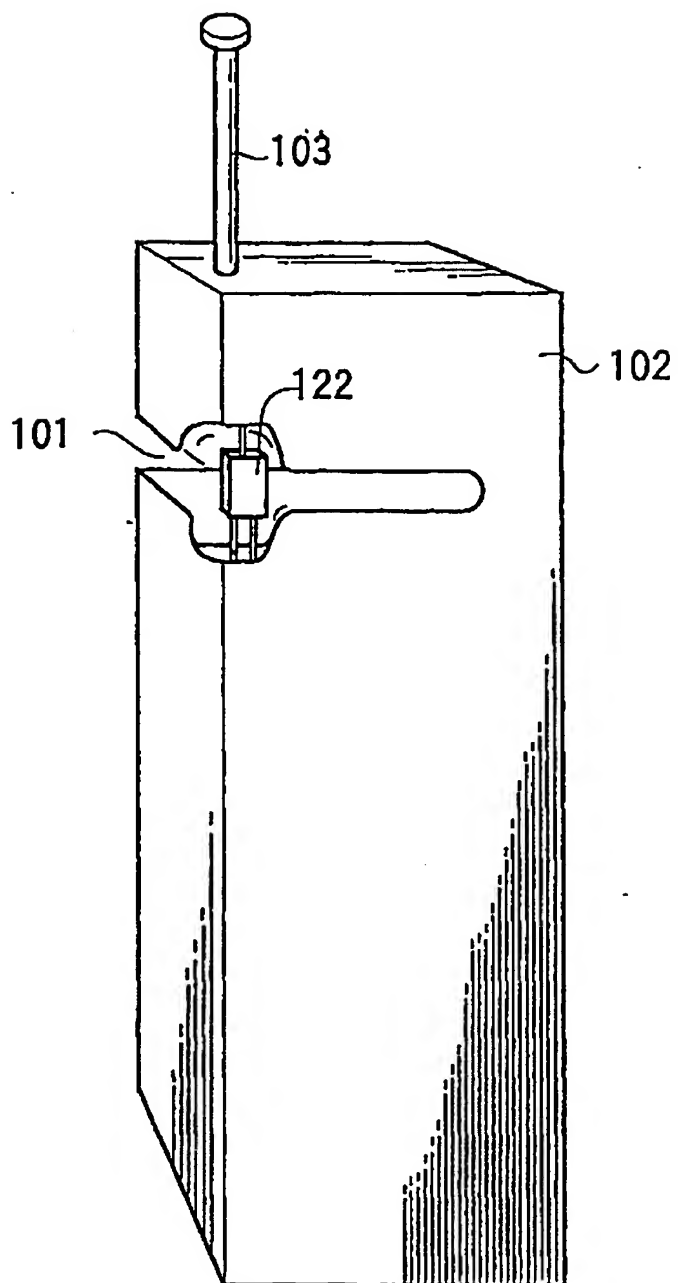


FIG. 43

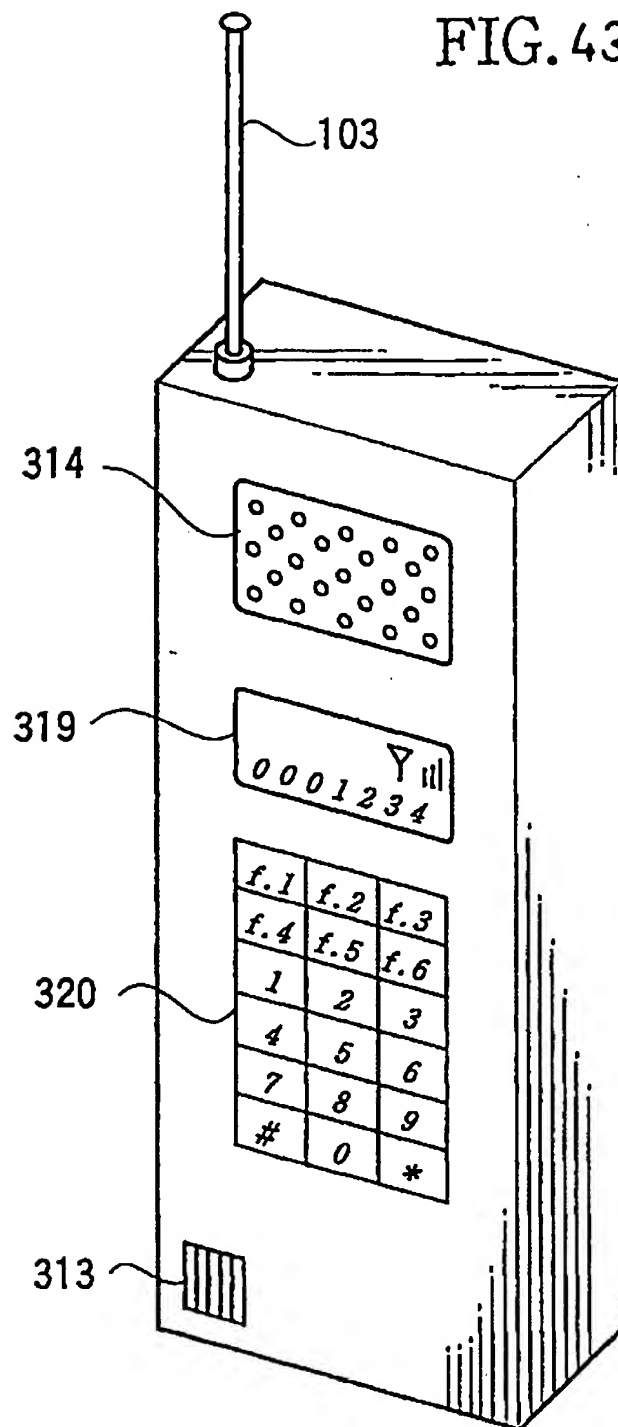


FIG. 44

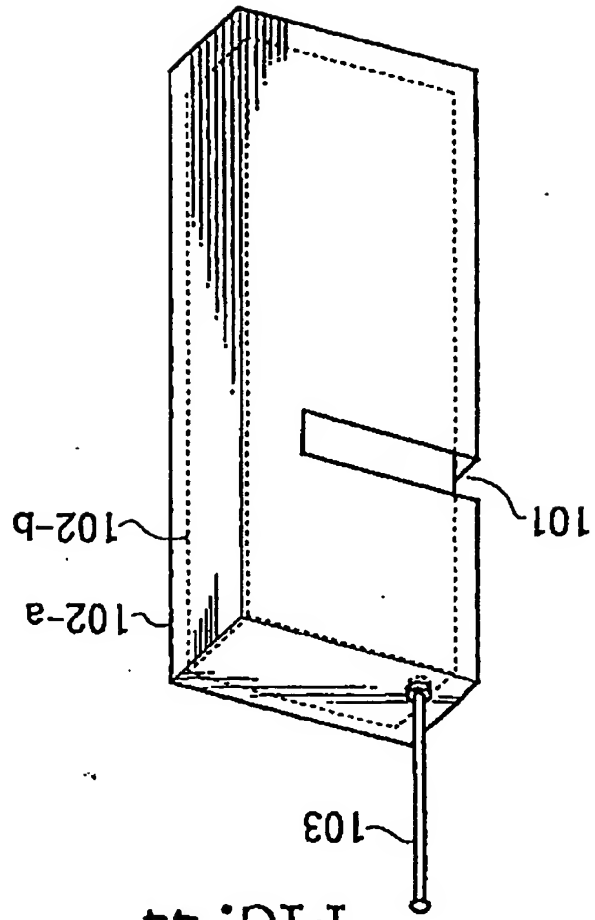


FIG. 45

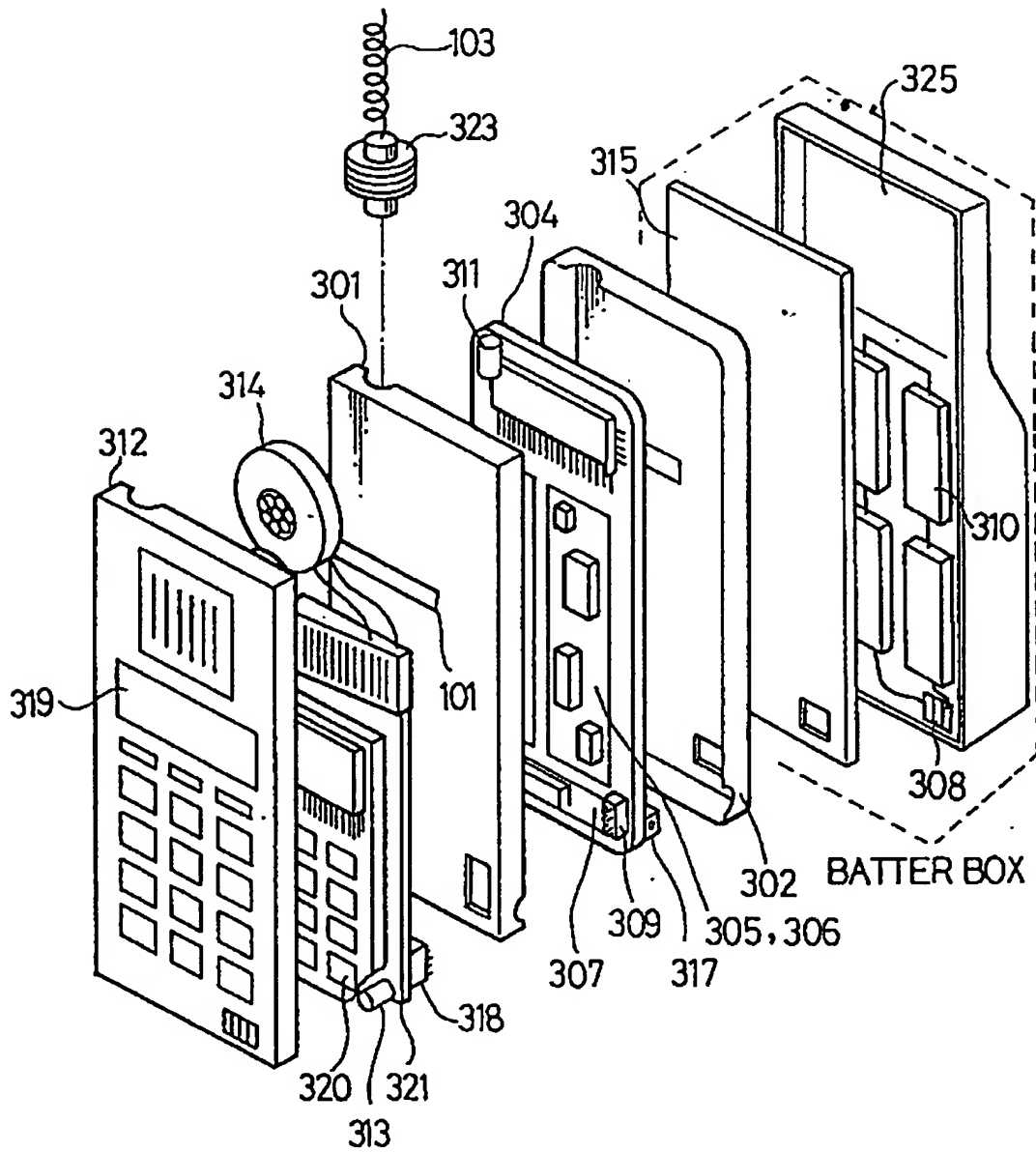


FIG. 46

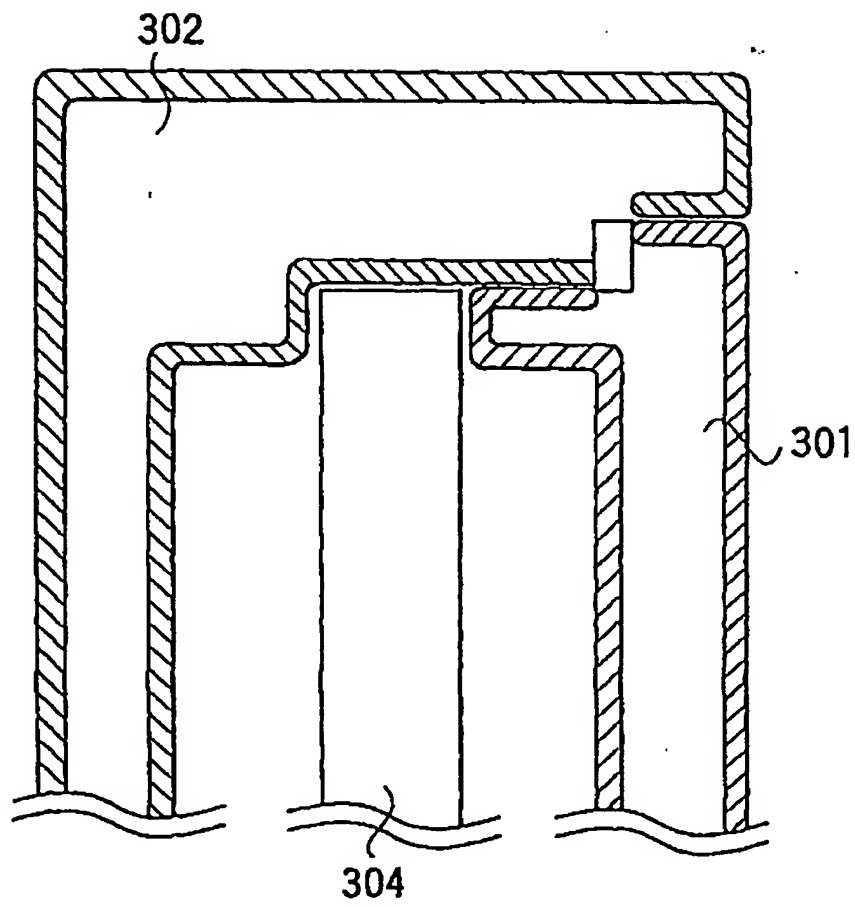


FIG. 47A

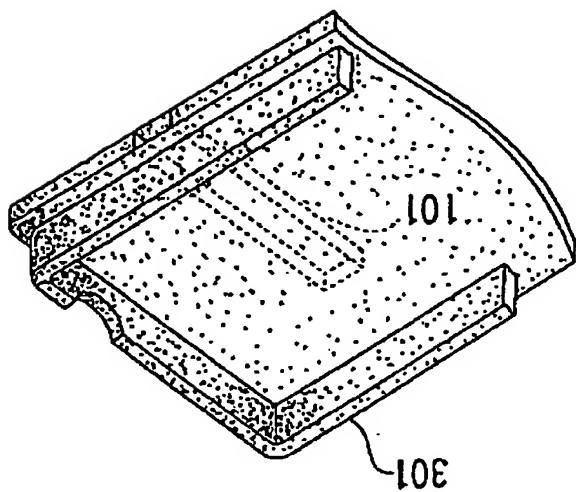


FIG. 47B

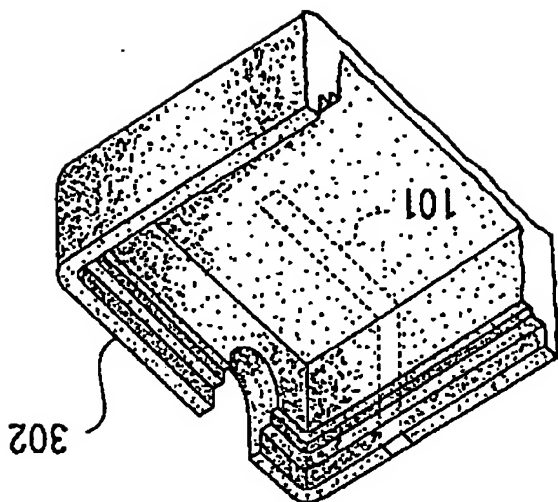


FIG. 48

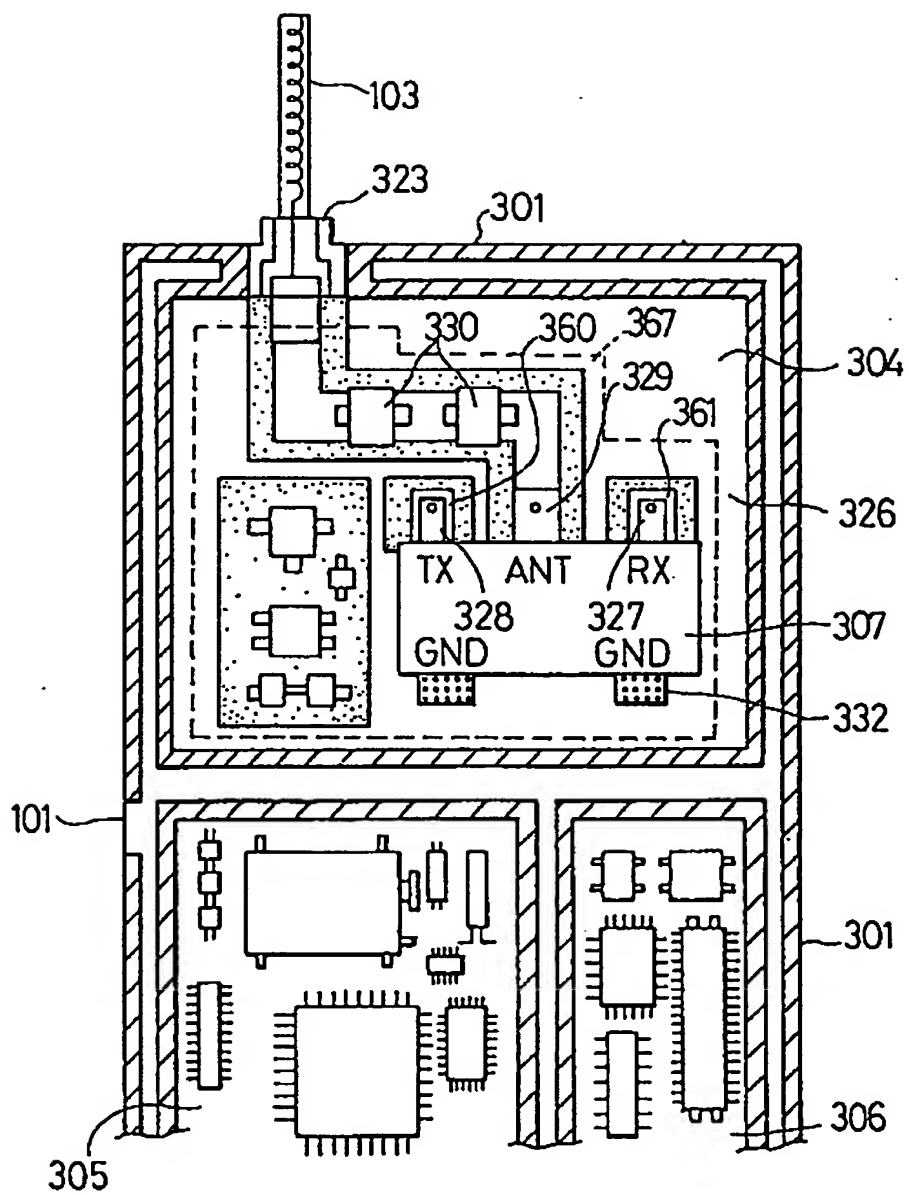


FIG. 49

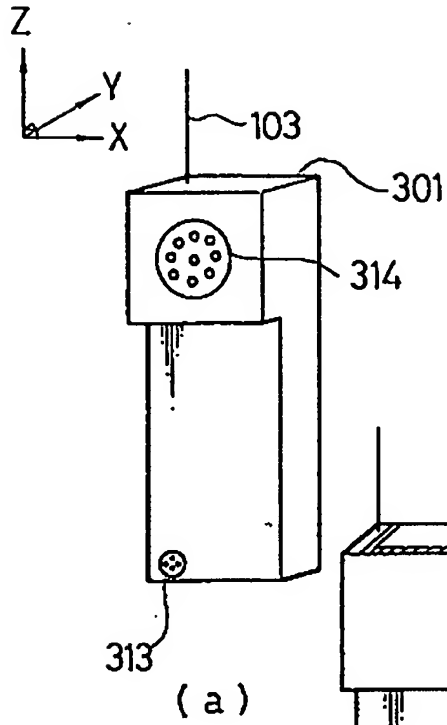


FIG. 50

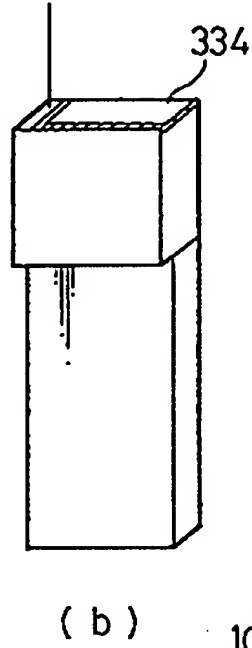


FIG. 51

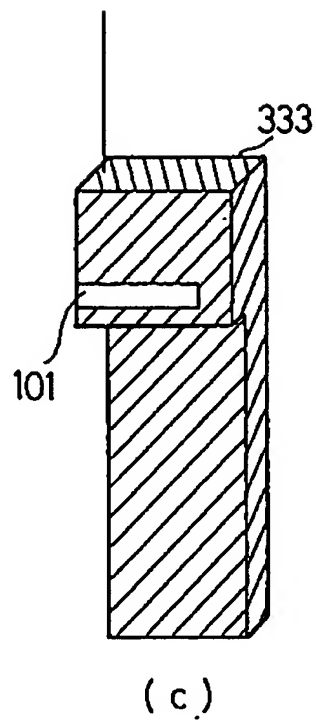


FIG. 52

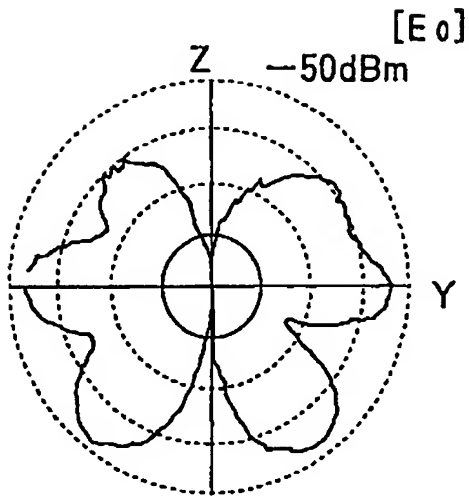


FIG. 53

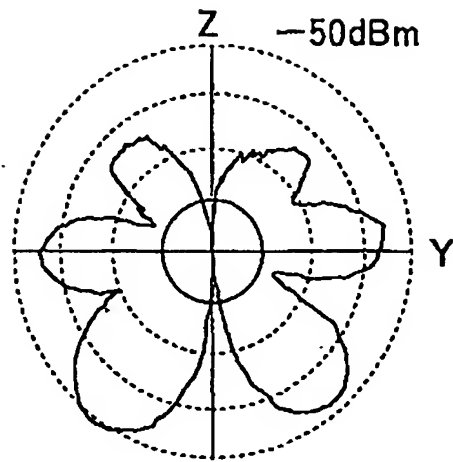


FIG. 54

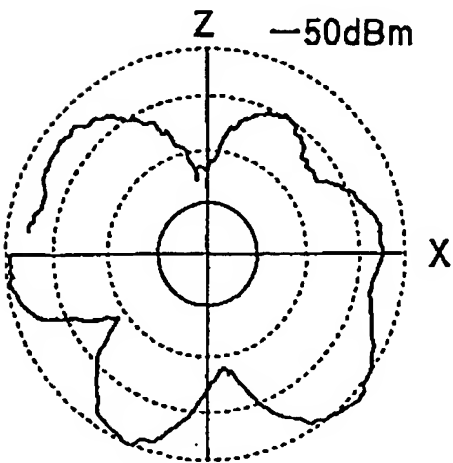


FIG. 55

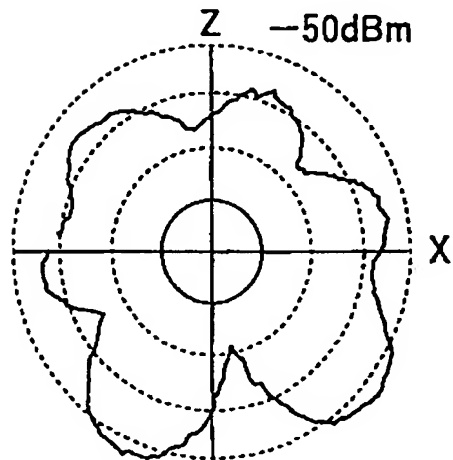


FIG. 56

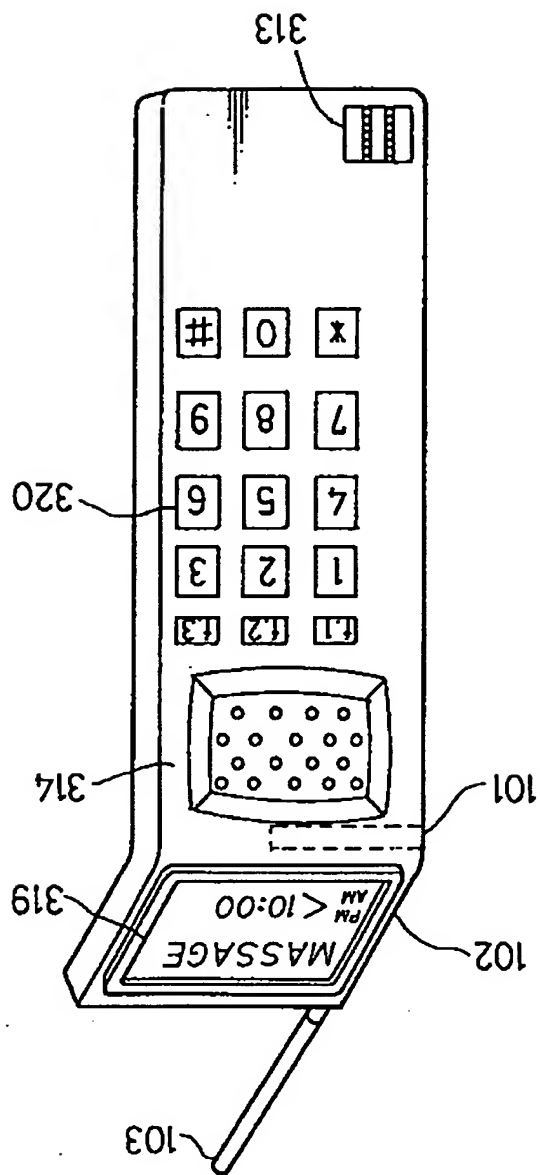


FIG. 57

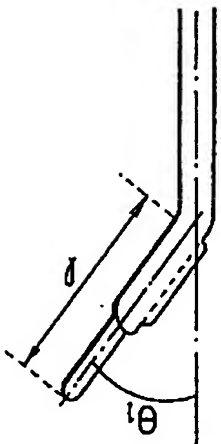


FIG.58A

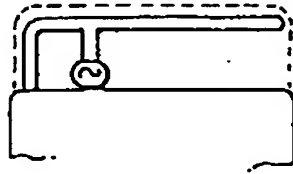


FIG.58B

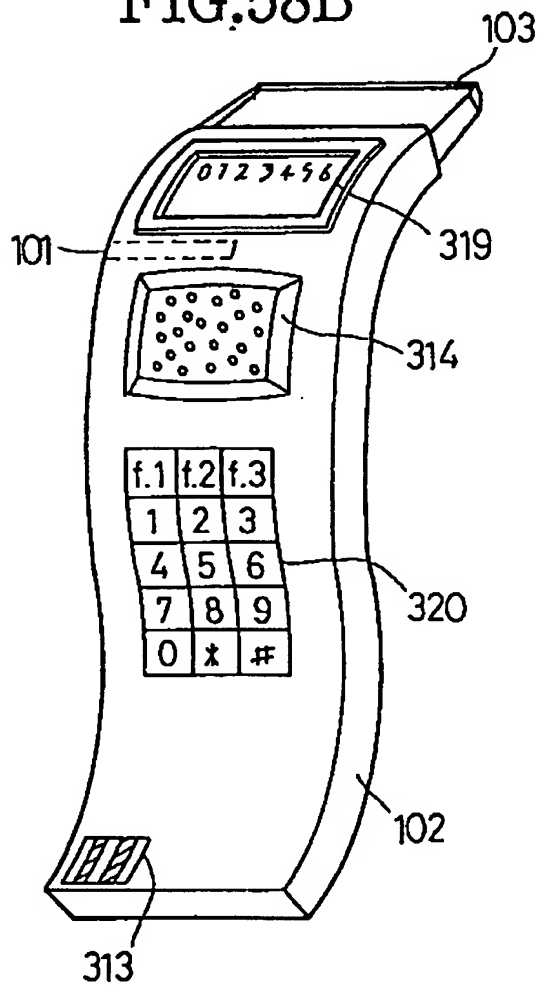


FIG.58C



FIG.59A

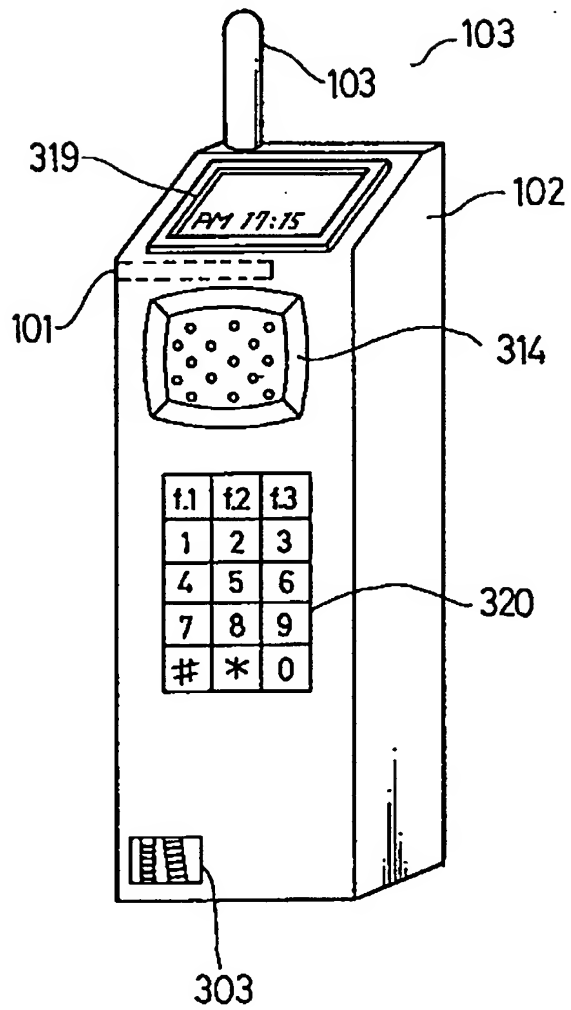


FIG.59B

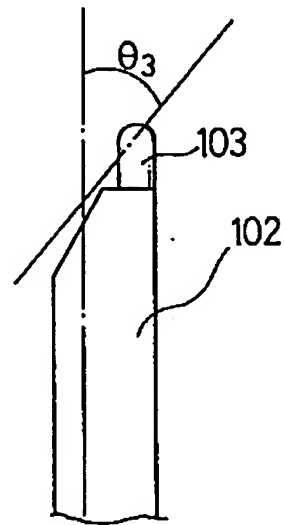


FIG. 60

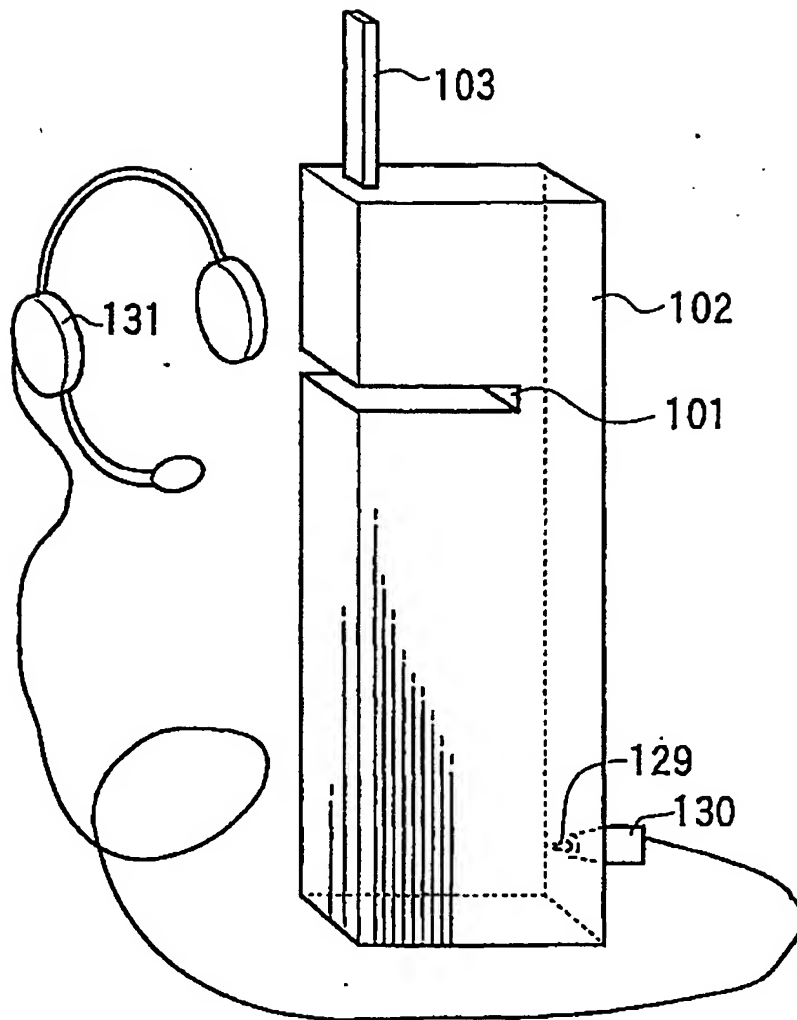


FIG. 61

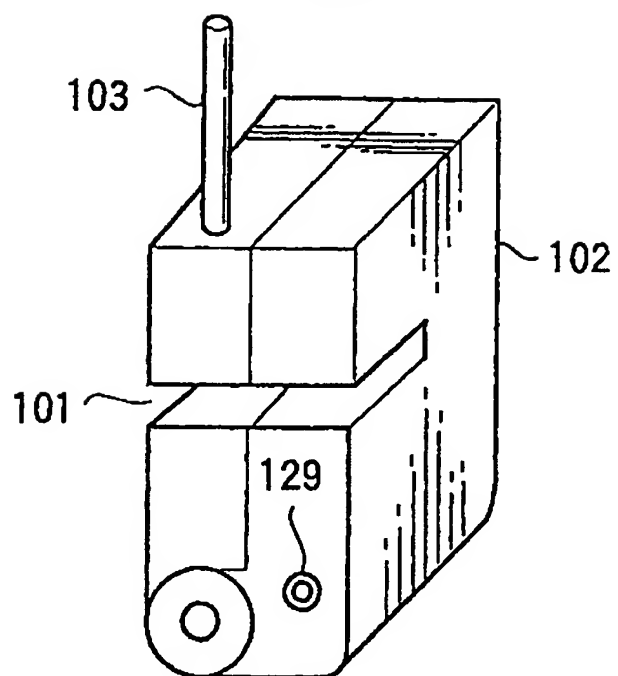
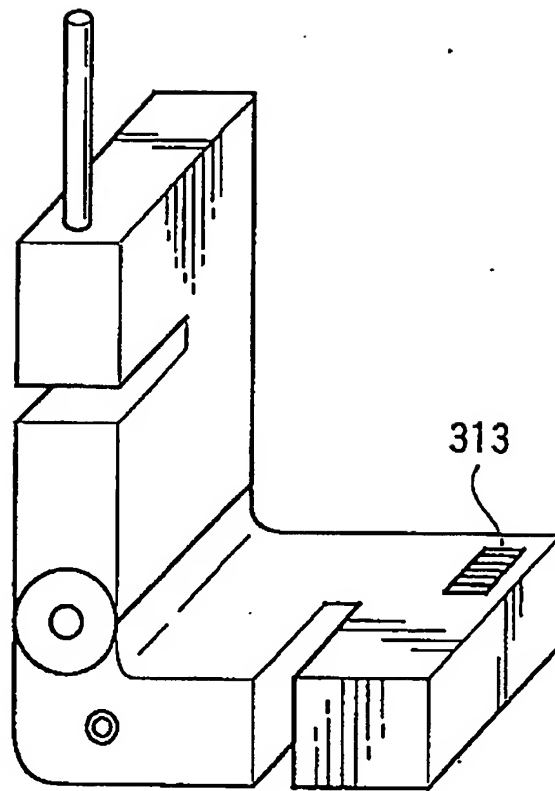


FIG.62



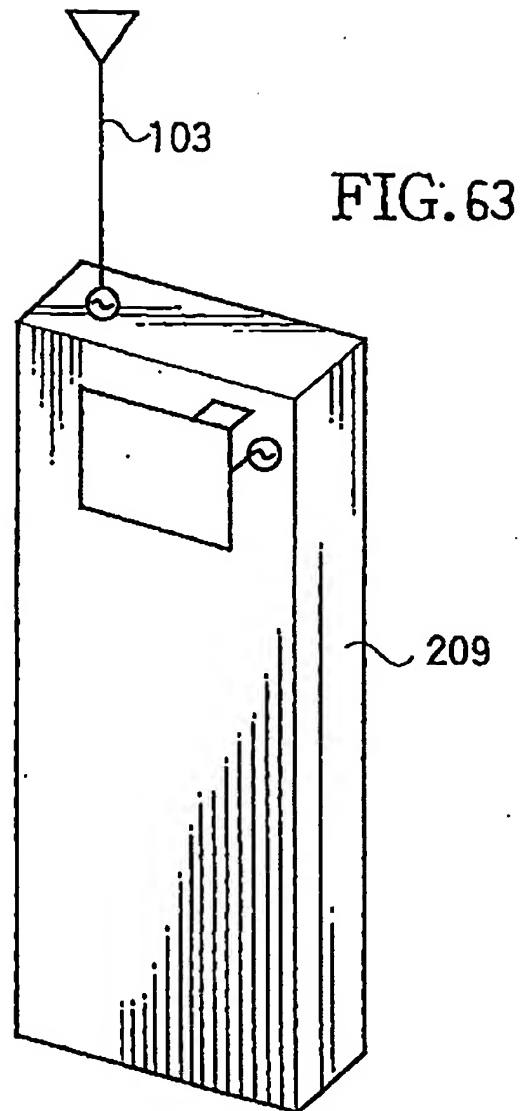


FIG. 64

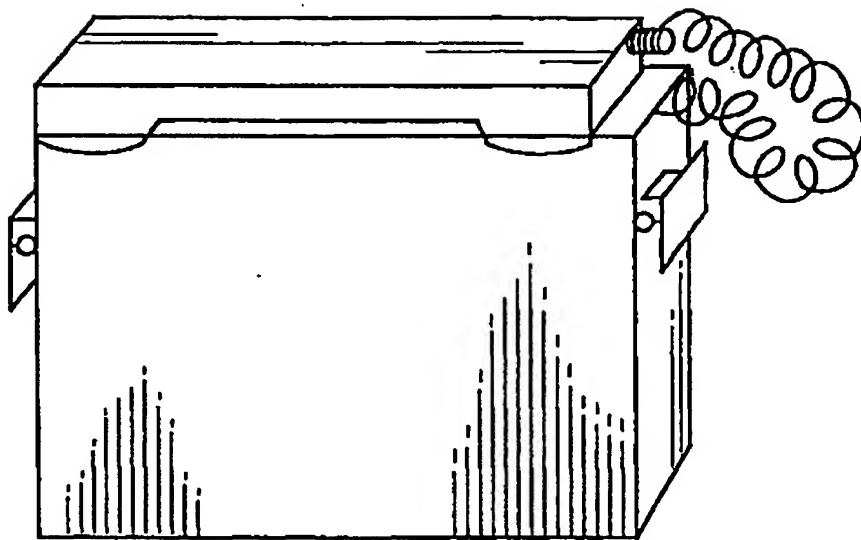


FIG. 65

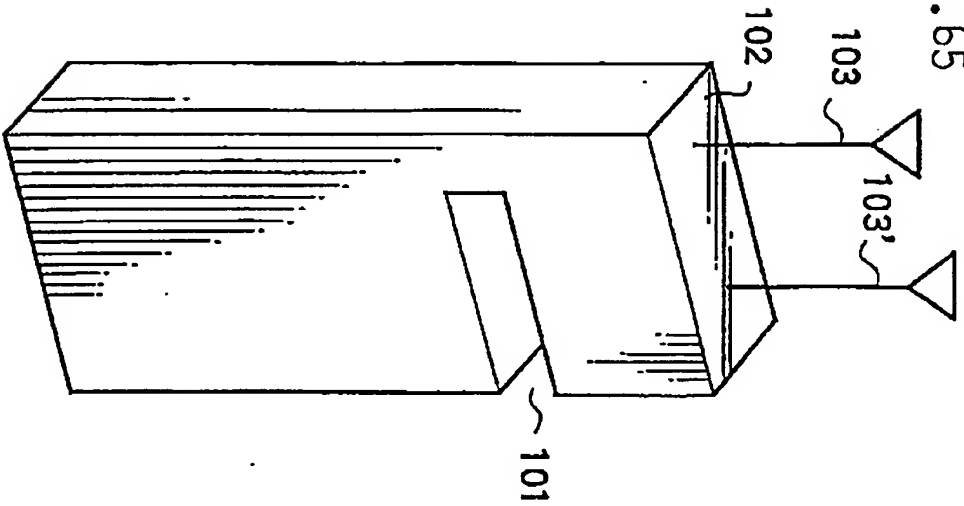


FIG. 66

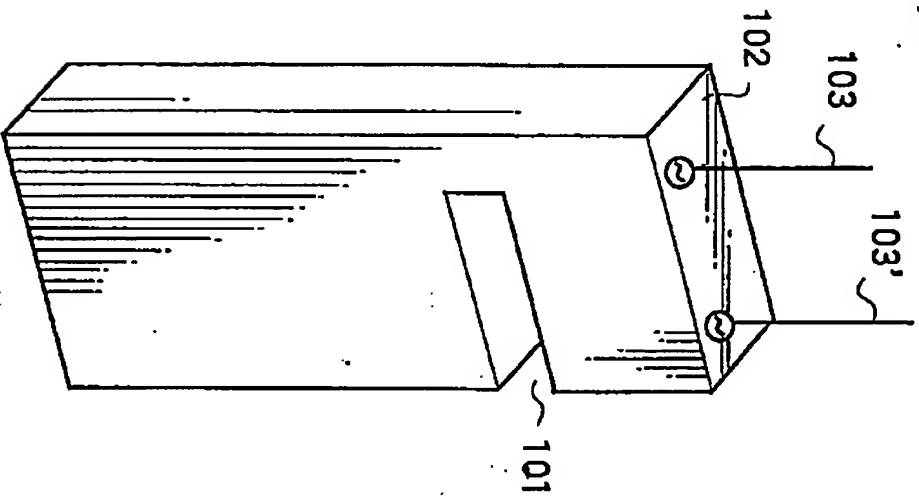


FIG. 67

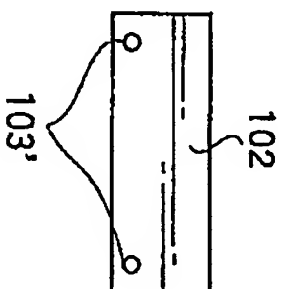


FIG.68A

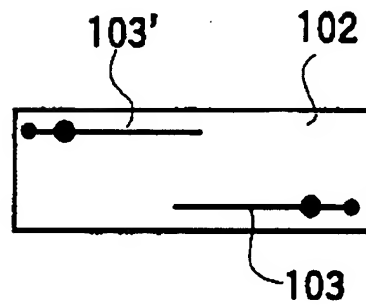


FIG.68B

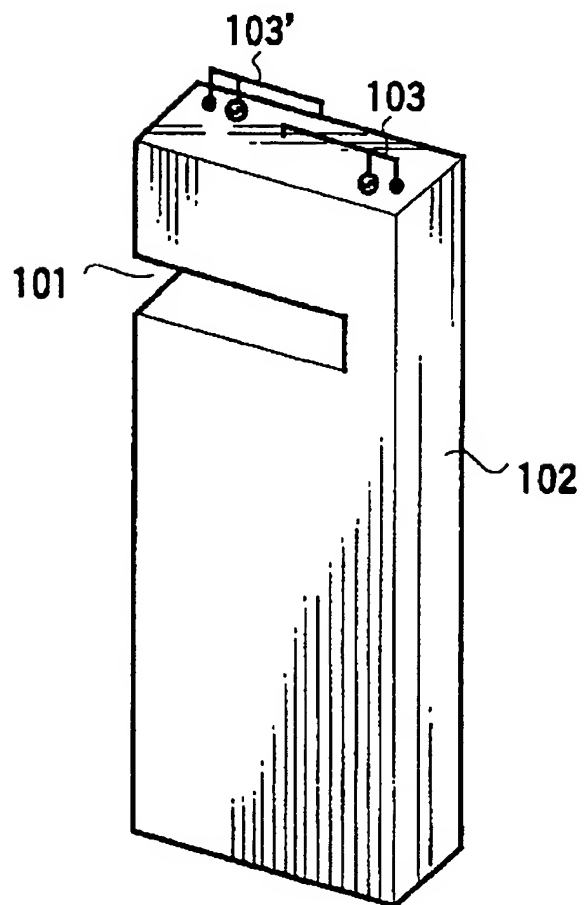


FIG. 69A

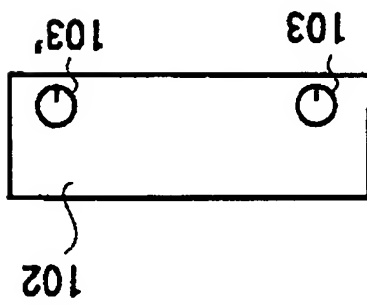


FIG. 69B

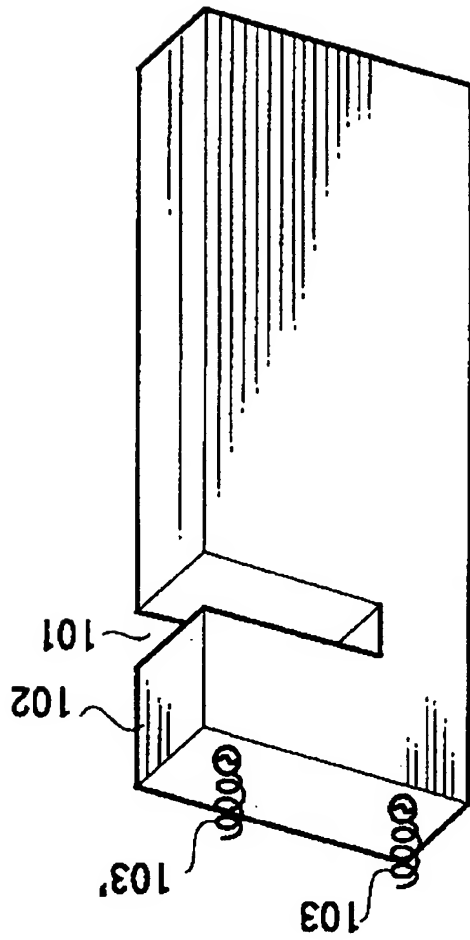


FIG.70

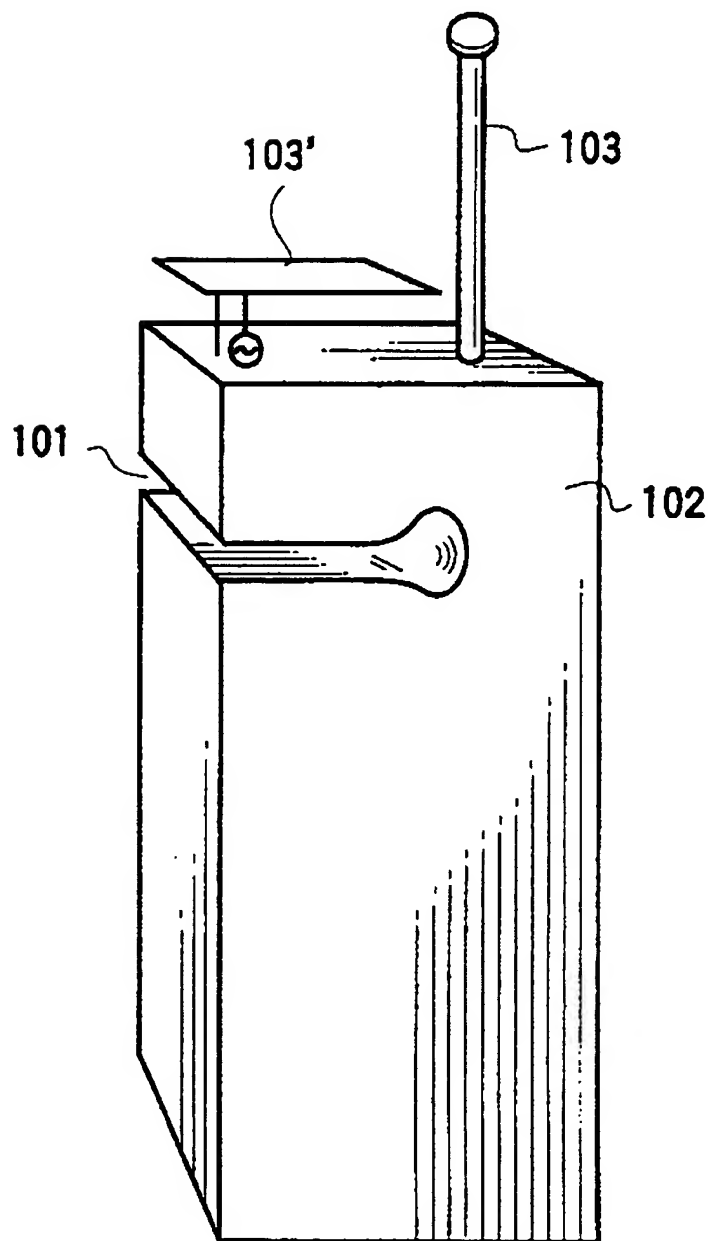


FIG.71

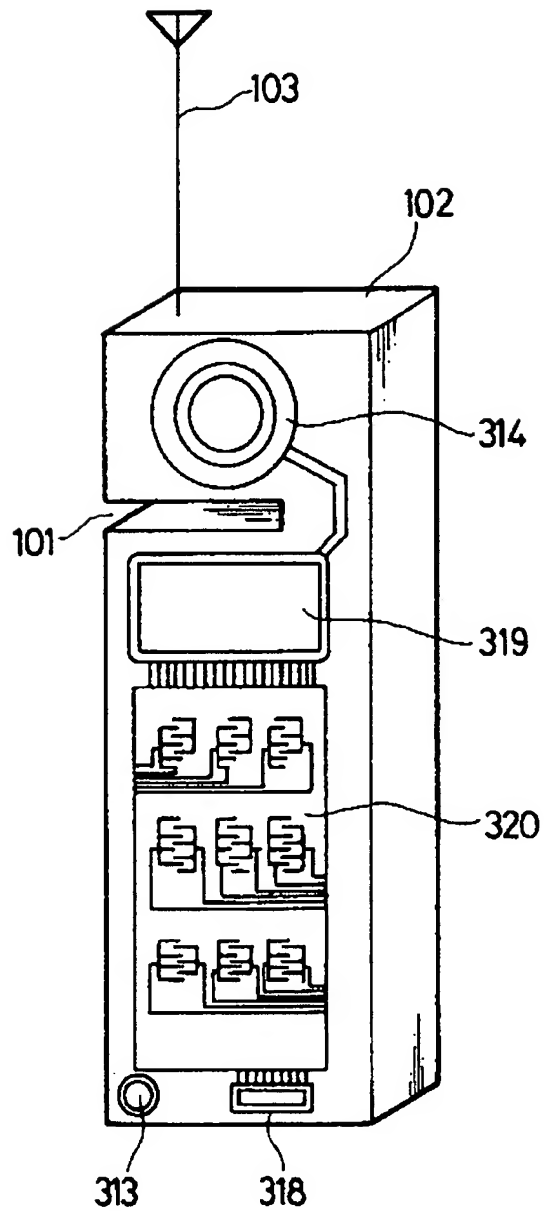


FIG.72

